

# Ultra-Thin and In-Parallel perfect sound absorbers

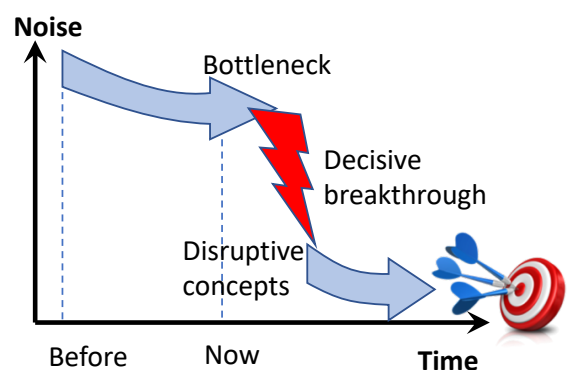
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## Introduction



**For a long time, humans have  
wanted to reduce aircraft noise ...**



## Introduction

Cutaway view of the air inlet with classical liner



New concepts of plane

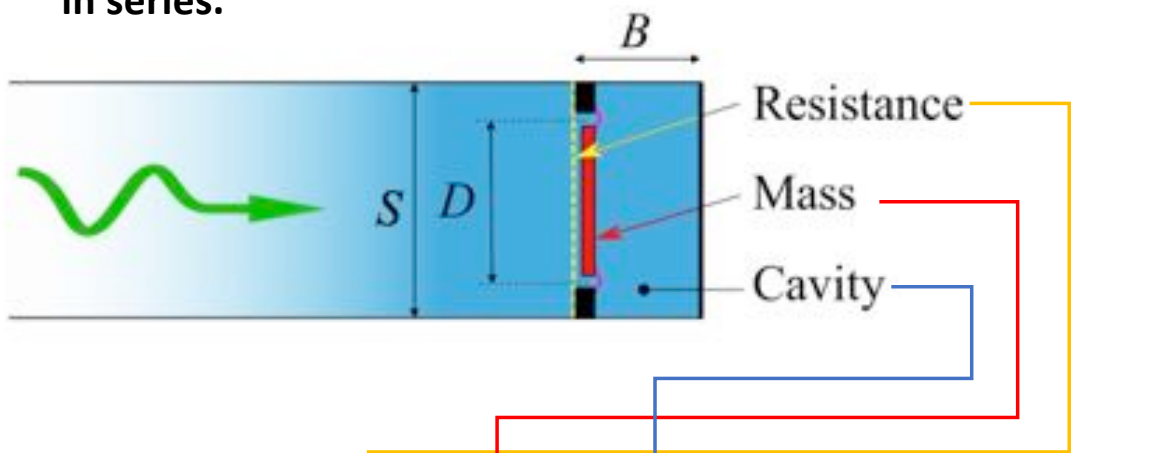


Need for high efficiency and new concepts



## Generalized Helmholtz Resonator

The generalized Helmholtz resonator (GHR) is composed of a moving mass, a spring due to the cavity and a resistance in series.



$$Z = \frac{p}{\rho_0 c_0 v} = \frac{R}{\sigma} + \frac{j\hat{\omega}L}{\sigma} + \frac{1}{j\hat{\omega}C}$$

$$\text{POA} = \sigma = \frac{A_D}{A_S}$$

$$\hat{\omega} = \frac{\omega}{\omega_c}$$

## Generalized Helmholtz Resonator

If the target is to have a perfect absorption  $Z = 1$   
when  $\omega = \omega_c$

The impedance can be written

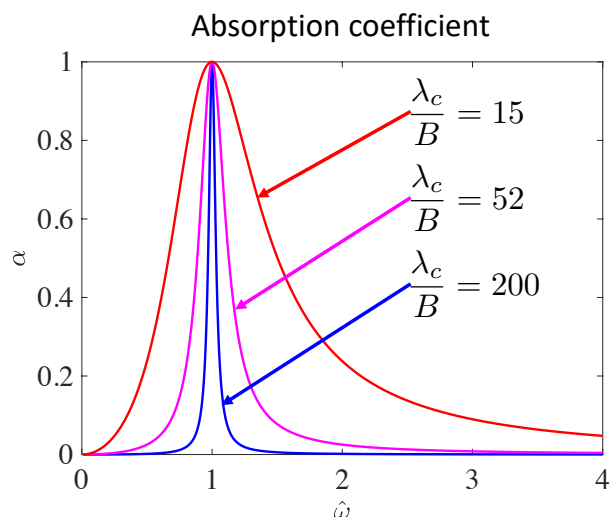
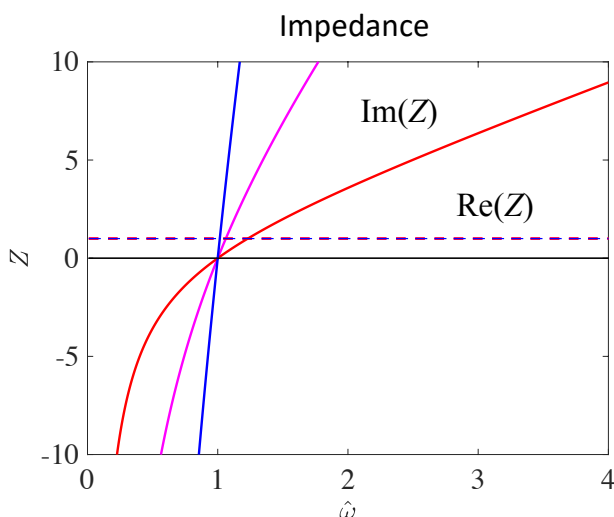
$$Z = 1 + \frac{1}{C} \left( j\hat{\omega} + \frac{1}{j\hat{\omega}} \right)$$

dependent on a single parameter  $C = 2\pi \frac{B}{\lambda_c}$

which is inversely proportional to the subwavelength ratio.

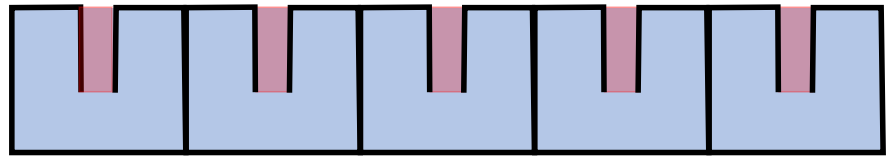
	$f_c = 650 \text{ Hz}$	$B = 35 \text{ mm}$	$\frac{\lambda_c}{B} = 15$
Examples:	$f_c = 650 \text{ Hz}$	$B = 10 \text{ mm}$	$\frac{\lambda_c}{B} = 52$
	$f_c = 170 \text{ Hz}$	$B = 10 \text{ mm}$	$\frac{\lambda_c}{B} = 200$

## Generalized Helmholtz Resonator

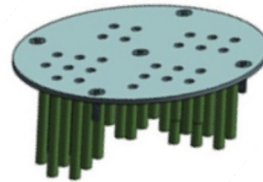


- It is possible to have perfect absorption at any frequency and at any cavity thickness.
- As the subwavelength ratio increases, the absorption peak becomes increasingly sharp.

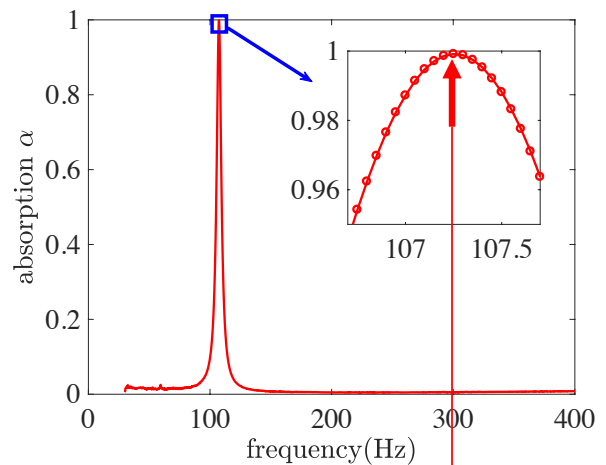
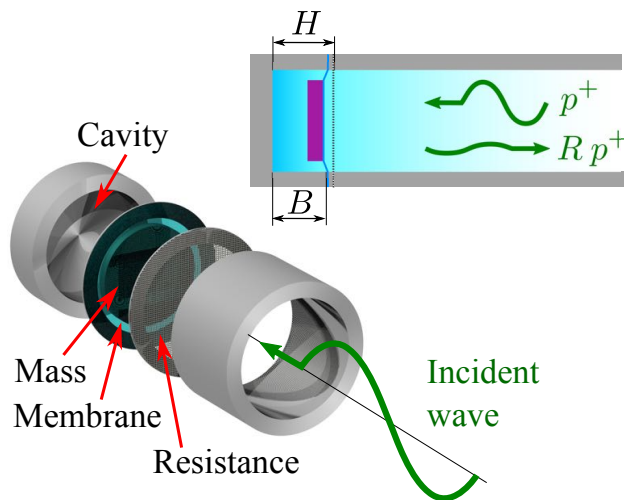
# Generalized Helmholtz Resonator



In classical Helmholtz resonator, the mass and the resistance are linked in the neck.



# Generalized Helmholtz Resonator



$$H = 16 \text{ mm}$$

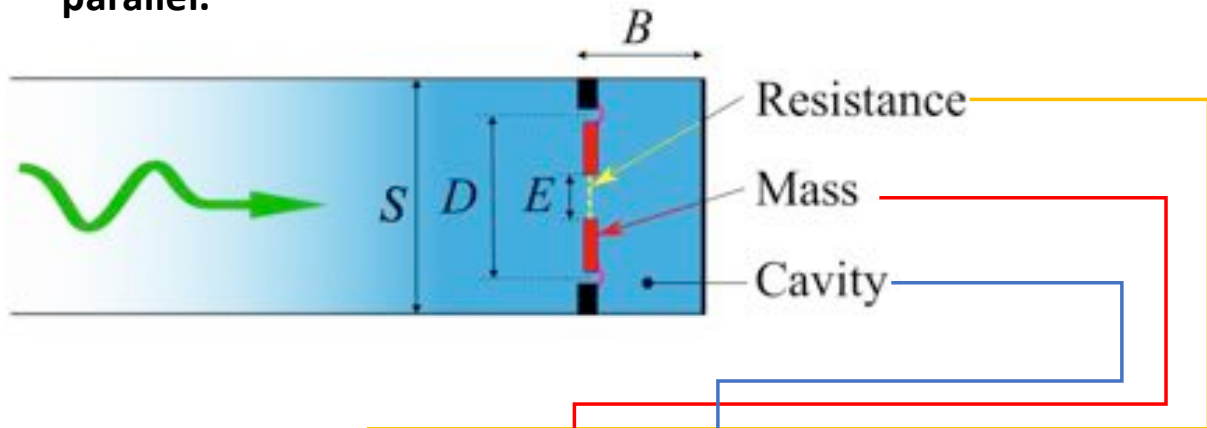
$$\lambda = 3.23 \text{ m} = 202 H$$



Aurégan, Y. (2018). Ultra-thin low frequency perfect sound absorber with high ratio of active area. *Applied Physics Letters*, 113(20), 201904.

## In parallel Helmholtz resonators

The in parallel Helmholtz resonator (IPHR) is composed of a spring due to the cavity, a moving mass and a resistance in parallel.



$$Z = \frac{1}{\frac{1}{R'} + \frac{1}{j\omega L'}} + \frac{1}{j\omega C}$$

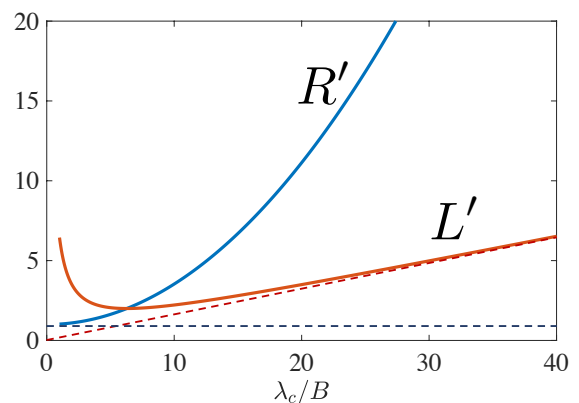
$R'$ ,  $L'$  take into account the POA

## In parallel Helmholtz resonators

If the target is to have a perfect absorption  $Z = 1$  when  $\omega = \omega_c$

The resistance and the inductance can be written

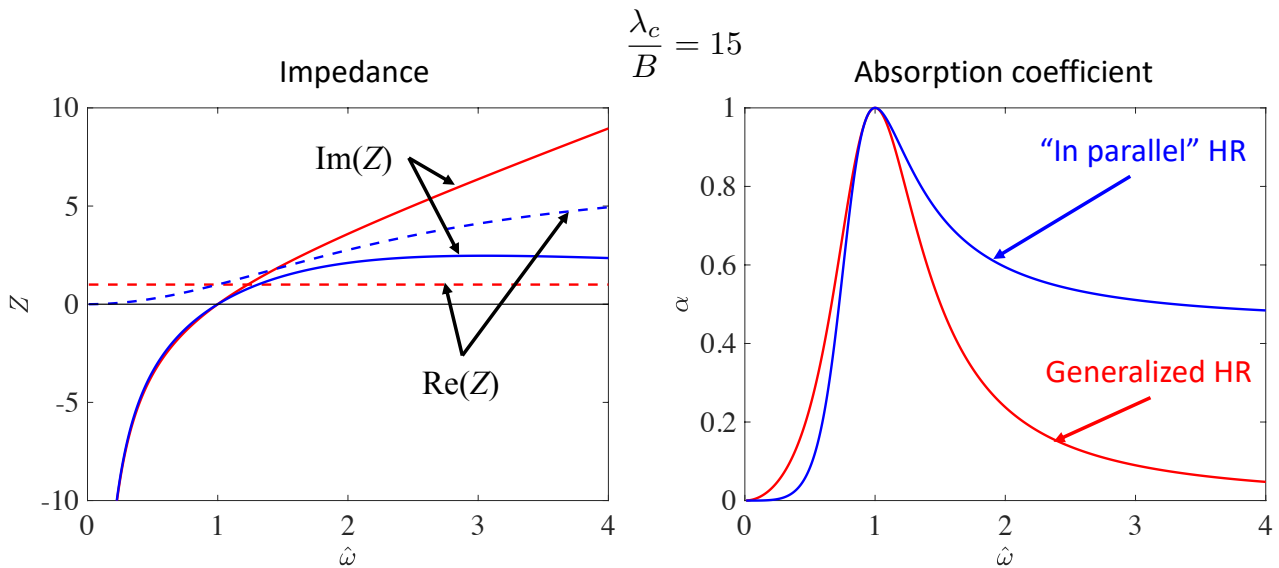
$$R' = \frac{1 + C^2}{C^2} \quad L' = \frac{1 + C^2}{C}$$



dependent on a single parameter  $C = 2\pi \frac{B}{\lambda_c}$

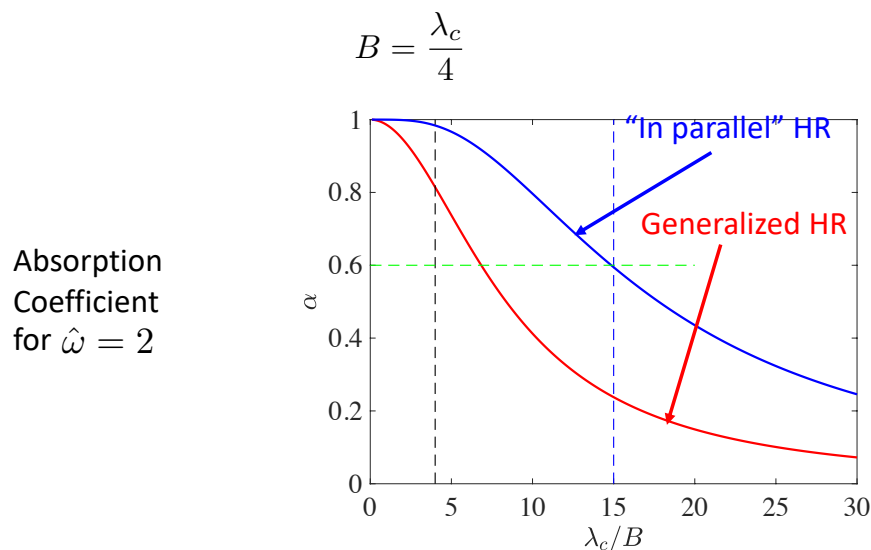
which is inversely proportional to the subwavelength ratio.

## “In parallel” Helmholtz resonators



- The “in parallel” HR can also have a perfect absorption at any frequency and at any cavity thickness.
- When the subwavelength ratio is not too high, the absorption is substantially higher at mid-frequencies with a IPHR than with a GHR.

## “In parallel” Helmholtz resonators

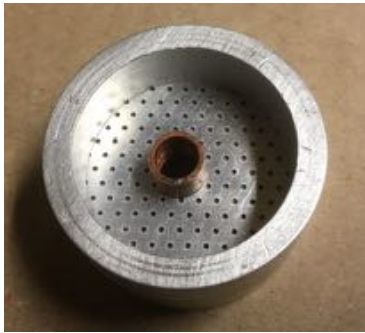


The “in parallel” HR increases the frequency band where the liner is efficient compared to the generalized HR.

Choice:  $\frac{\lambda_c}{B} = 15 \rightarrow R' = 6.70$       Choice:  $f_c = 650 \text{ Hz}$   
 $L' = 2.81$        $B = 35 \text{ mm}$

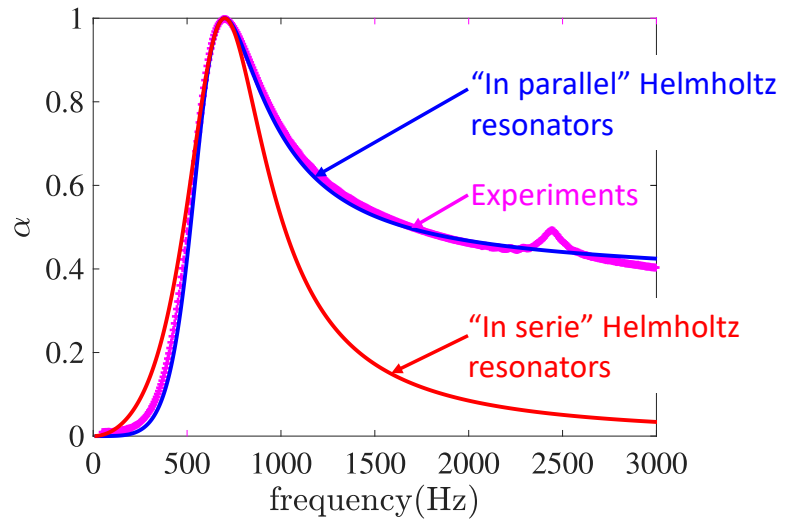
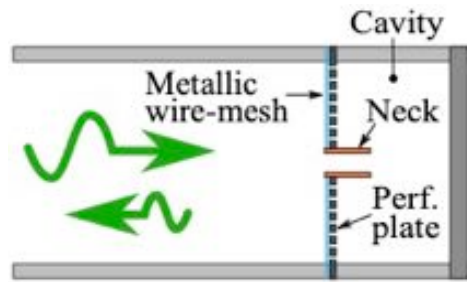


## “In parallel” Helmholtz resonators



$$B = 30 \text{ mm}$$

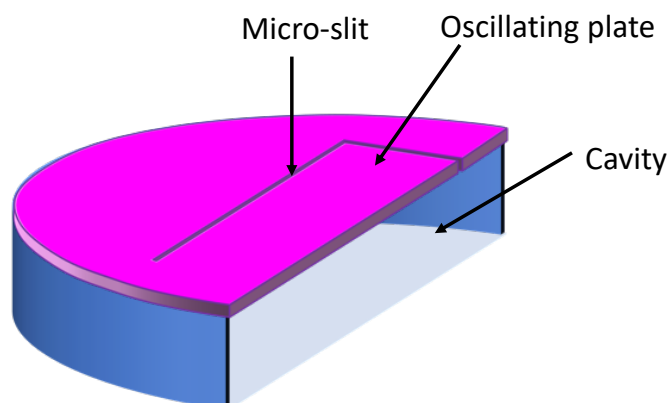
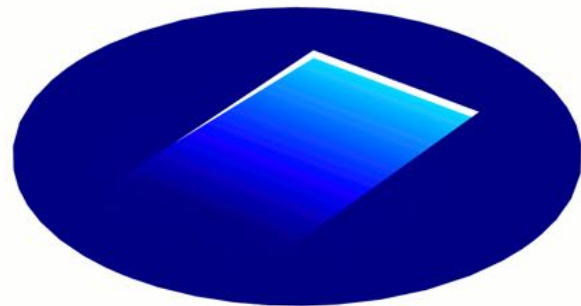
$$\frac{\lambda_c}{B} = 16.4$$



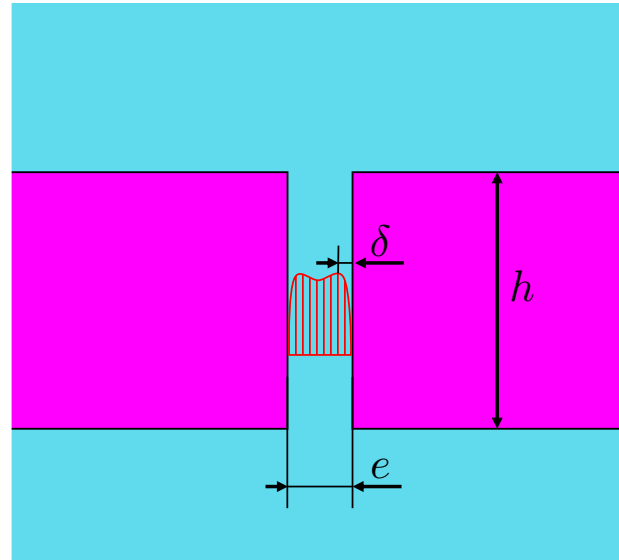
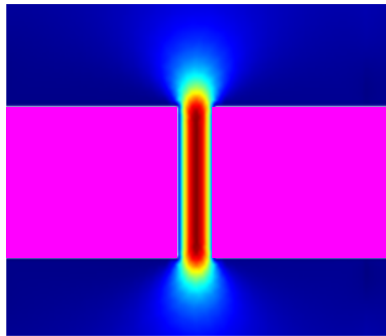
Aurégan, Y., & Farooqui, M. (2019). In-parallel resonators to increase the absorption of subwavelength acoustic absorbers in the mid-frequency range. *Scientific reports*, 9(1), 11140.

## “In parallel” Helmholtz resonators

- A bending beam is more suitable with flow
- Avoid adding stiffness to the system



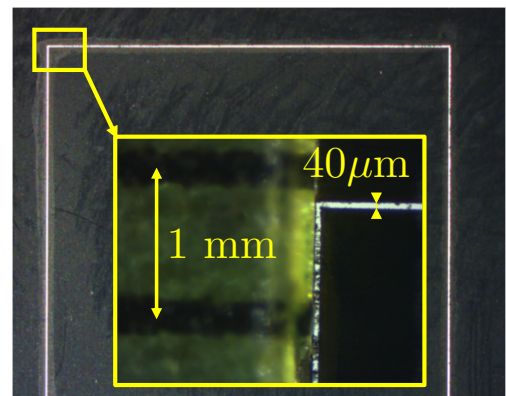
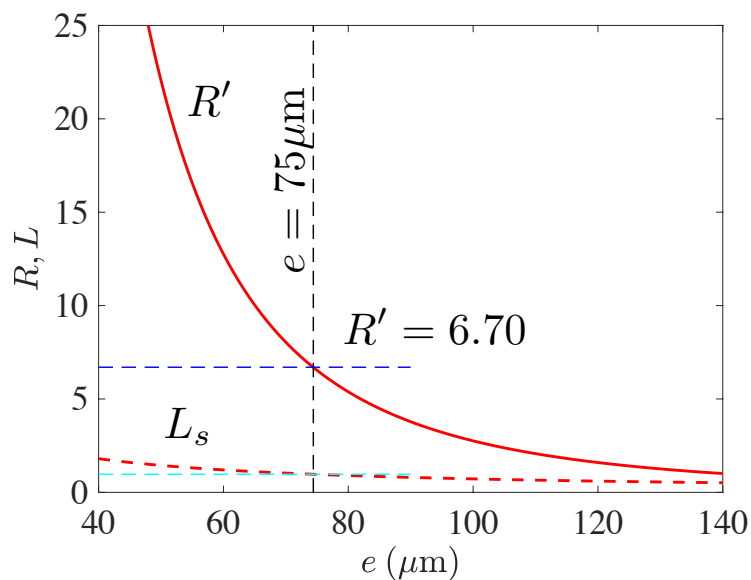
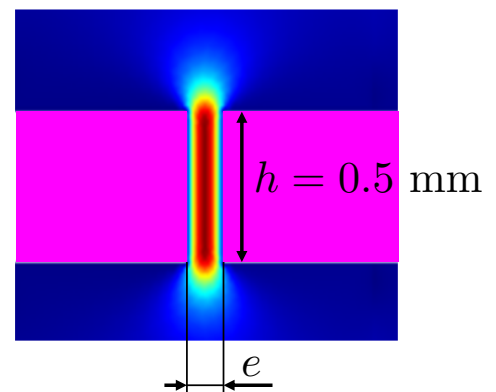
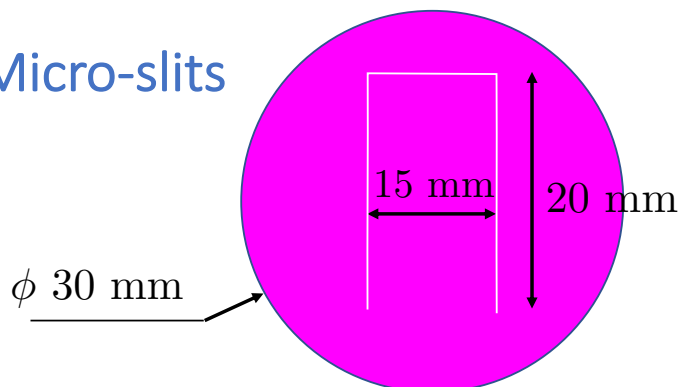
## Micro-slits



$$j\omega\rho_0 h\bar{v} = \left(1 - \frac{\tanh(\gamma e/2)}{\gamma e/2}\right) \Delta p \quad \gamma = \frac{1+j}{\delta} \quad \delta = \sqrt{\frac{2\mu}{\omega\rho_0}}$$

$$Z_s = j \frac{S}{S_s} \frac{\omega h}{c_0} \left(1 - \frac{\tanh(\gamma e/2)}{\gamma e/2}\right)^{-1}$$

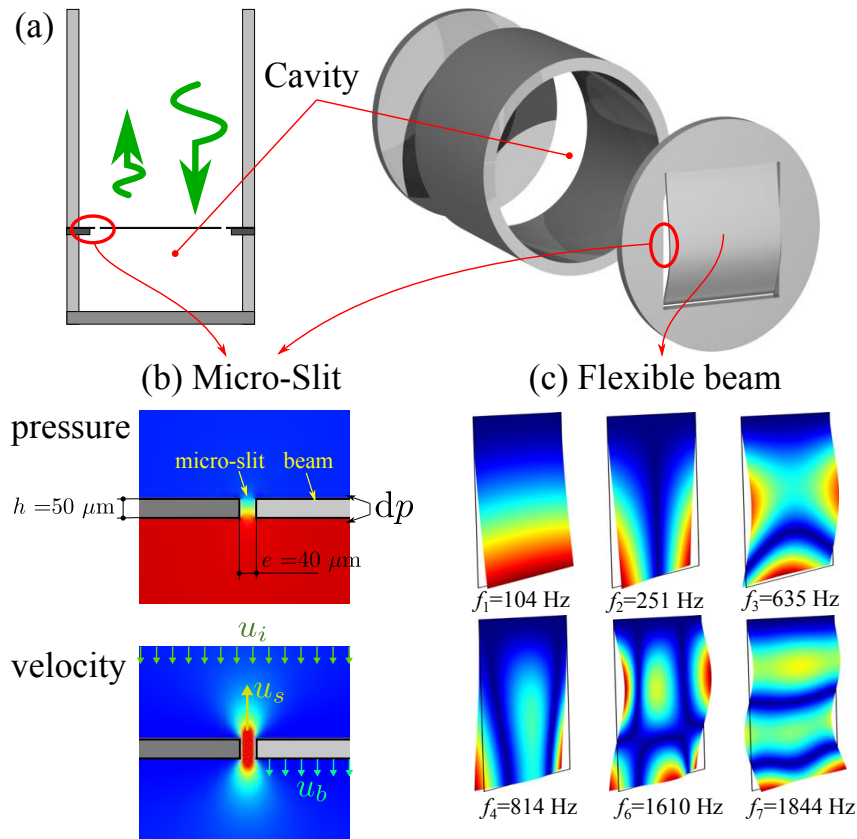
## Micro-slits



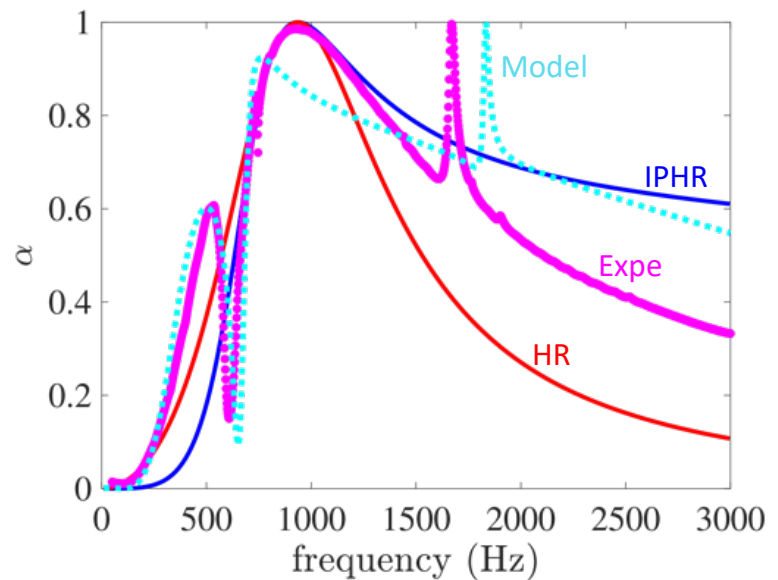
$POA_{\text{slit}} = 0.9\%$



# “In parallel” Helmholtz resonators with micro-slits

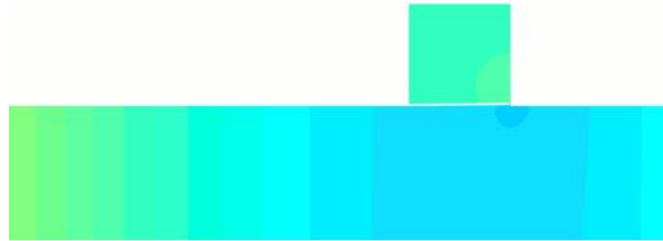


# “In parallel” Helmholtz resonators with micro-slits



## Perspectives

- Use the cantilever beam with micro-slit material in a duct wall with flow



- Transformation in a semi-active system

