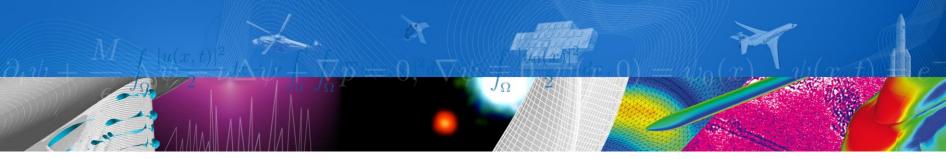


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Advanced identification techniques and design tools applied to innovative aeroacoustic liners

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- Context
- Liner design strategy
- Uncertainty quantification
- Illustration on recent ONERA activities



fan

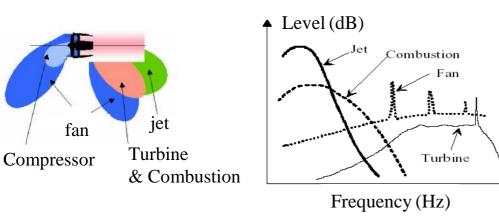
Use of liners in nacelle of aircraft engines to reduce fan, turbine and combustion noise



zero-spliced liners - A380 (Journal Aerospace Lab (7) 2014)

Use of liners in wing leading edge to reduce interaction noise

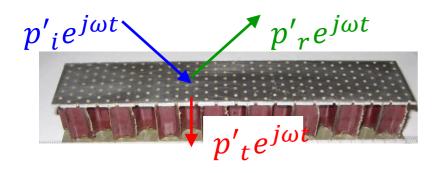




Use of liners along a duct to reduce jet pump noise



Classical liners concepts



Locally reacting behavior

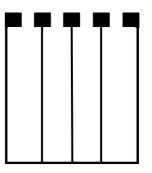
Surface impedance:

6

$$Z(\omega) = \frac{p'}{\boldsymbol{v}'.\boldsymbol{n}}$$

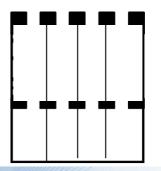
$$Z(\omega) = R(\omega) + jX(\omega)$$

• Single Degree of Freedom liner (**SDOF**): 1 resistive layer (~porous) above 1 cavity (reactive)



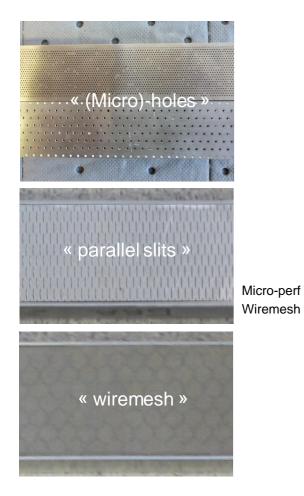
→ Absorption in a narrow frequency band

Double Degree of Freedom liner (DDOF):
2 resistive layers and 2 cavities



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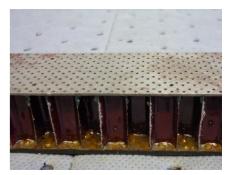
Resistive layers

7

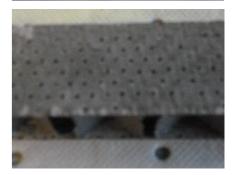


SDOF









Honeycomb cells

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New challenges for noise mitigation with acoustic liners

UHBR engines



Urban air-taxi



Distributed Electrical Propulsion



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Game-changer in manufacturing process: "3D printing"

Sintering

9

creating a solid mass using heat without liquefying it. Metal powders (DMLS) or thermoplastic powders (SLS)

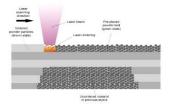
Direct Metal Laser Melting (DMLM) and Electron Beam Melting (EBM)

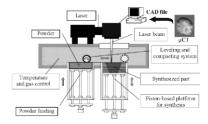
fully melting of materials through laser or electron beam. Ideal for manufacturing dense, non-porous objects.

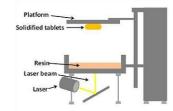
• Stereolithography (SLA)

photopolymerization to print ceramic or polymer objects

Radical opening of the design-space for acoustic liner concepts

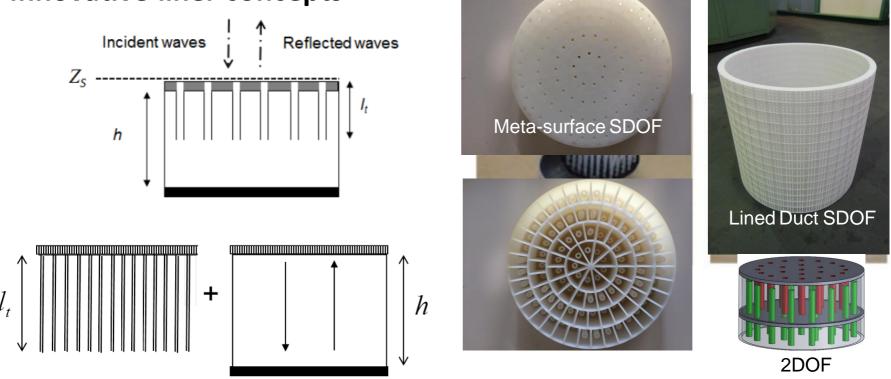








Innovative liner concepts



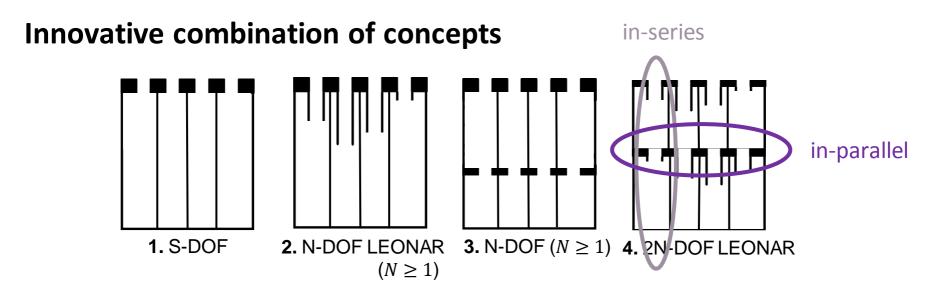
LEONAR concept:

- Radical decrease of the resonance frequency through the prolongation of propagation length (effect on reactance)
- Increase of the absorption coefficient at low frequencies by prolongation of tube length (added resistance)

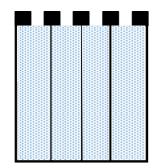
Ref: Simon et al in ICA 2013 / Inter.noise 2016 / ICSV24 / Inter.noise 2018 / J. Sound Vib., 421, 1-16, (2018)

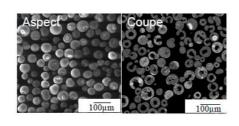
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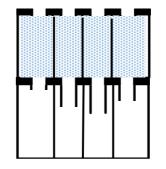
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Insertion of foam (classical or advanced internal structure)







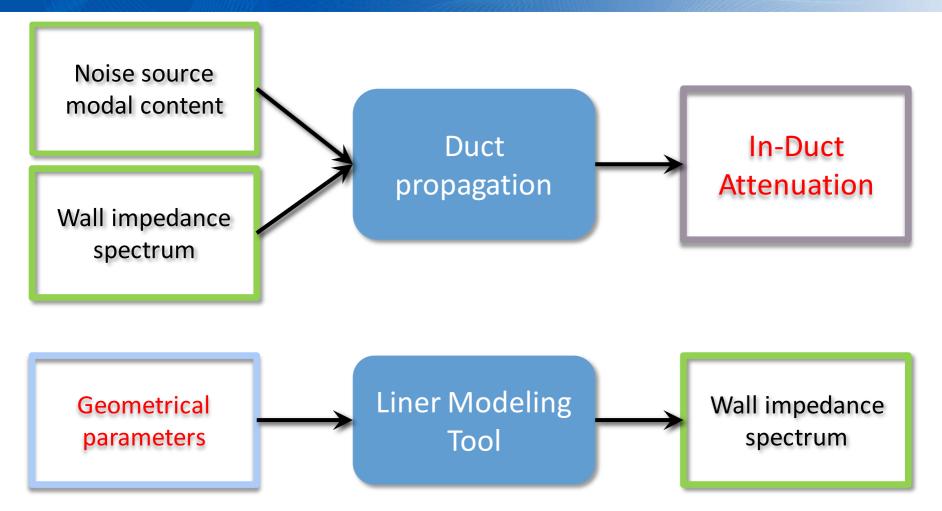




- Liner design strategy
- Uncertainty quantification
- Illustration on recent ONERA activities



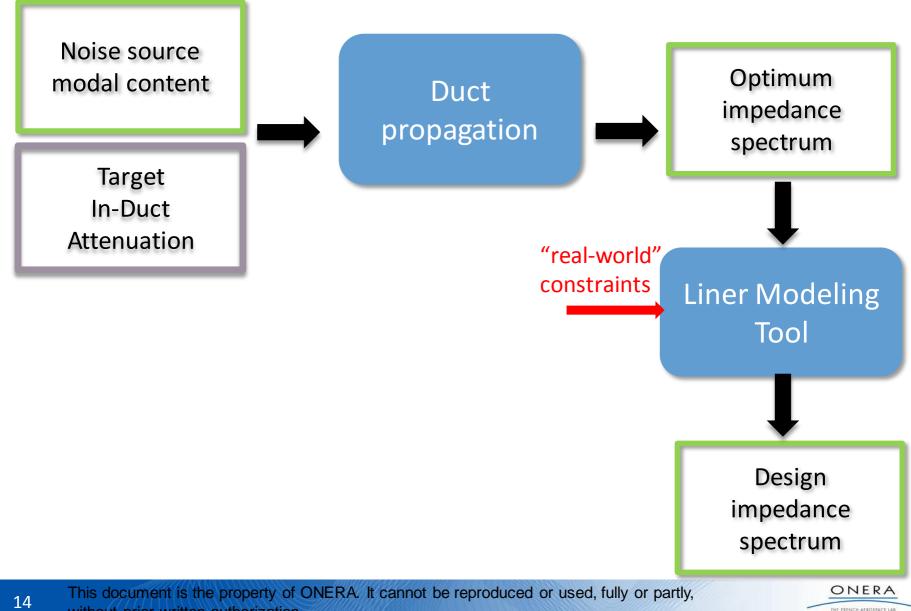
Liner design strategy



Objective: find the liner design which will yield the targeted in-duct attenuation

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Typical industrial requirements

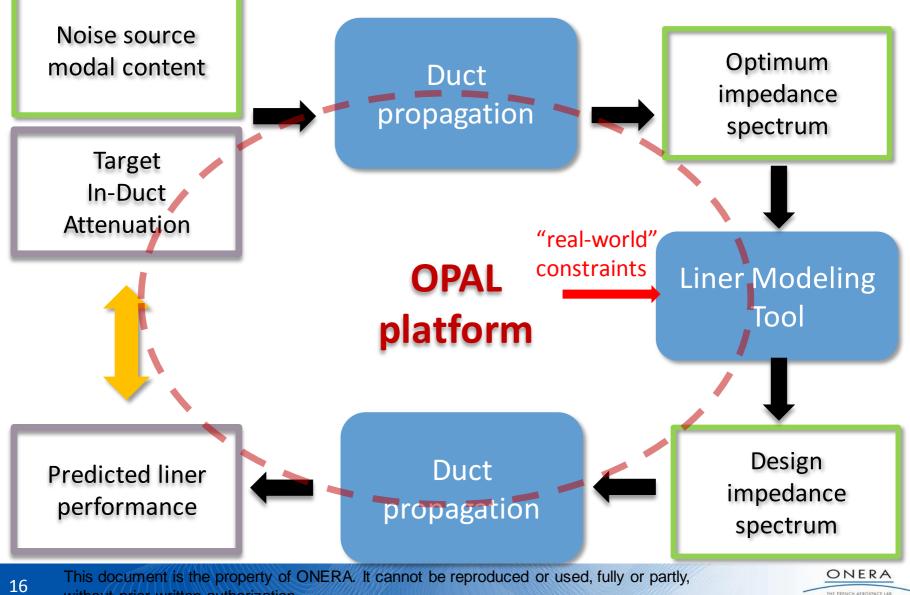
RTCA DO-160G (FAA and EUROCAE). « Environmental Conditions and test Procedures for Airborne Equipment »

- Section 4 : Temperature and Altitude
- Section 5 : Temperature variation
- Section 6 : Humidity
- Section 8 : Vibration
- Section 10 : Waterproofness
- Section 11 : Fluid susceptibility
- Section 12 : Sand and dust
- Section 14 : Salt fog

Example of requirements for engine noise mitigation:

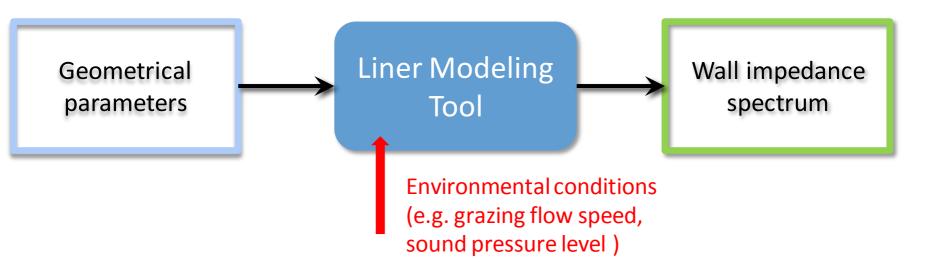
- · Aerodynamic behaviour: negligible impact
- Weight: max 8kg/m²
- Temp.: max 600-650 °C
- Mach: 0.5-0.6
- Fatigue strength, vibration, thermal cycle, thermal gradient, fire, drainage, 100000 200000 h
- Manufacturing costs

Area	Air inlet	Cold duct downstream	Hot nozzle	Hot plug duct
Max thickness (mm)	50	20-30	15	200
Optimum Impedance Spectrum	R/ρc: 2 to 3 X/ρc: -0.5 to -1	R/ρc: 1 to 1.5 X/ρc: 0 to -0.6	R/ρc: 1 to 2 X/ρc: 0 to -0.5	R/ρc: 0.5 to 1.5 X/ρc: 0 to -0.3



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Key element: liner modeling tool



Basis of most liner modeling tools: **semi-empirical models** fitted on experimental results.

Example for a perforated plate (Kirby & Cummings 1998, Malmary et. al 2001):

$$Z = \frac{\sqrt{2\nu\omega}}{\sigma c_0} \frac{h}{\delta} + \left[26,16 \left(\frac{h}{2\delta}\right)^{-0,169} - 20 \right] \frac{\nu^*}{\sigma c_0} - 0,645 \frac{\omega h}{\sigma c_0} + \frac{4}{3\pi} \frac{1 - \sigma^2}{\sigma c_0 C_D^{-2}} |\boldsymbol{\nu}'.\boldsymbol{n}| + j \frac{\omega}{\sigma c_0} \left[h + \frac{16\delta}{3\pi} \right]$$

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How are the semi-empirical impedance models derived?

→ impedance eduction

• Direct impedance measurement (e.g. Kirby & Cummings 1998)

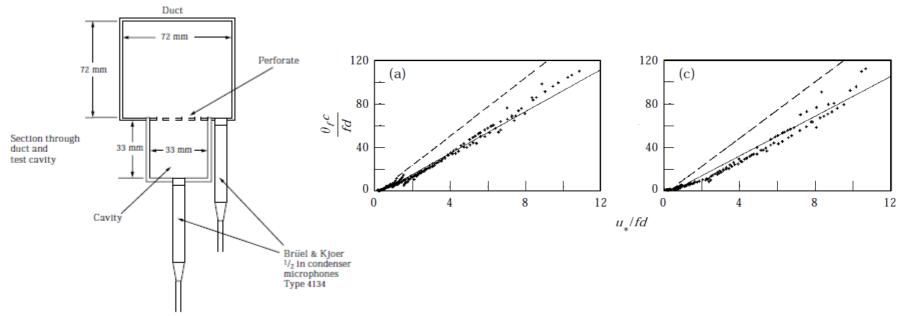


Figure 1. Apparatus for the measurement of the acoustic impedance of a perforate.

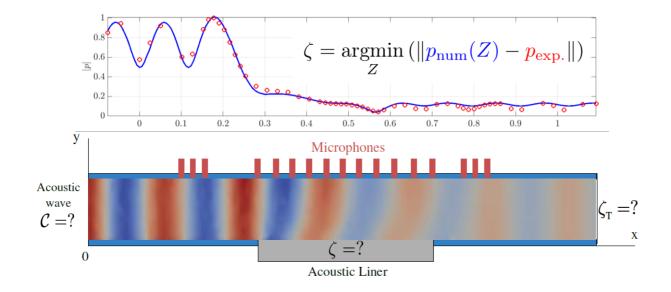
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How are derived the semi-empirical impedance models?

→ impedance eduction

- Direct impedance measurement (e.g. Kirby & Cummings 1998)
- Indirect methods (e.g. NASA, LAUM, DLR, ONERA, KTH...)





How are derived the semi-empirical impedance models?

→ impedance eduction

- Direct impedance measurement (e.g. Kirby & Cummings 1998)
- Indirect methods (e.g. NASA, LAUM, DLR, ONERA, KTH...)

→ fit on experimental data to derive a multi-parameter model

$$Z = \frac{\sqrt{2\nu\omega}}{\sigma c_0} \frac{h}{\delta} + \left[26,16 \left(\frac{h}{2\delta}\right)^{-0,169} - 20 \right] \frac{\nu^*}{\sigma c_0} - 0,645 \frac{\omega h}{\sigma c_0} + \frac{4}{3\pi} \frac{1 - \sigma^2}{\sigma c_0 C_D^{-2}} |\boldsymbol{\nu}'.\boldsymbol{n}| + j \frac{\omega}{\sigma c_0} \left[h + \frac{16\delta}{3\pi} \right] \frac{\nu^*}{\sigma c_0} + \frac{16\delta}{\sigma c_0} \left[h + \frac{16\delta}{3\pi} \right] \frac{\nu^*}{\sigma c_0} \frac{\nu^*}{$$

Two questions arise:

- what is the sensitivity of the impedance to the model formulation?
- what is the sensitivity of the impedance to an error in the model parameters?

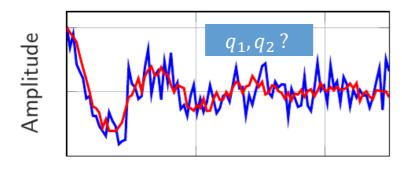
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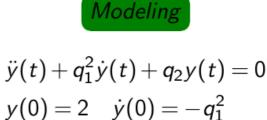
Key issue: dealing with the uncertainty



- Liner design strategy
- Uncertainty quantification
- Illustration on recent ONERA activities







Time

Deterministic $\boldsymbol{q}_{\text{optim}} = \arg\min_{\boldsymbol{q}} \left(\|\boldsymbol{y} - \boldsymbol{y}_{\text{exp}}\|_2 + r(\boldsymbol{x}) \right)$

- Ill-posedness of inverse problems : non-uniqueness, instability
- No uncertainty quantification

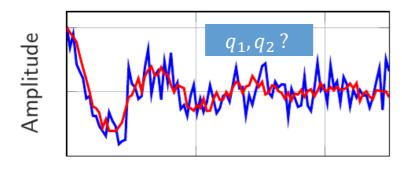
22

A posteriori : given y_{exp} , what probability density for (q_1, q_2) ?

$$\boldsymbol{\pi}(q|y_{exp}) = \frac{\overbrace{\boldsymbol{\pi}(y_{exp}|q)}^{\text{Likelihood Prior}}}{\boldsymbol{\pi}(y_{exp})} \qquad \boldsymbol{\pi}(y_{exp}|q) = \prod_{j} \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{|y_{exp}(t_j) - y(t_j)|^2}{2\sigma^2}\right)$$

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$$\ddot{y}(t) + q_1^2 \dot{y}(t) + q_2 y(t) = 0$$

 $y(0) = 2 \quad \dot{y}(0) = -q_1^2$

Time

Deterministic $\boldsymbol{q}_{\text{optim}} = \arg\min_{\boldsymbol{q}} \left(\left\| y - y_{\text{exp}} \right\|_2 + r(\boldsymbol{x}) \right)$

- Ill-posedness of inverse problems : non-uniqueness, instability
- No uncertainty quantification

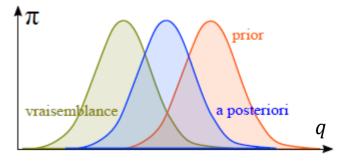
23

A posteriori : given y_{exp} , what probability density for (q_1, q_2) ?

$$\pi(q|y_{exp}) = \frac{\underset{\pi(y_{exp}|q)}{\underset{\pi(y_{exp})}{\underset{\pi(y_{ex$$



 $\boldsymbol{\pi}(q|y_{exp}) = \frac{\overbrace{\boldsymbol{\pi}(y_{exp}|q)}^{\text{Likelihood Prior}}}{\boldsymbol{\pi}(y_{exp})}$



How to sample from $\pi(q|y_{exp})$ without knowing $\pi(y_{exp})$?

→ Monte Carlo Markov Chain strategy

Random-walk generation of $y^{(k)}$ samples by exploring the space of $q \rightarrow$ creation of a Markov Chain whose stationary distribution is $\pi(q|y_{exp})$

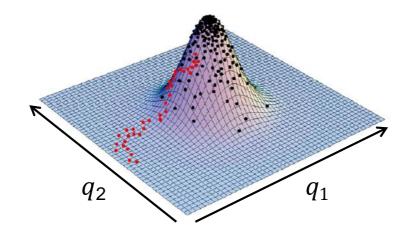
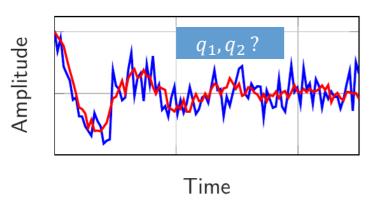
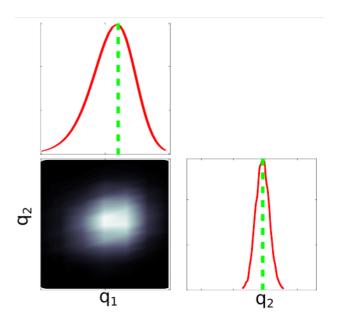


Illustration of results



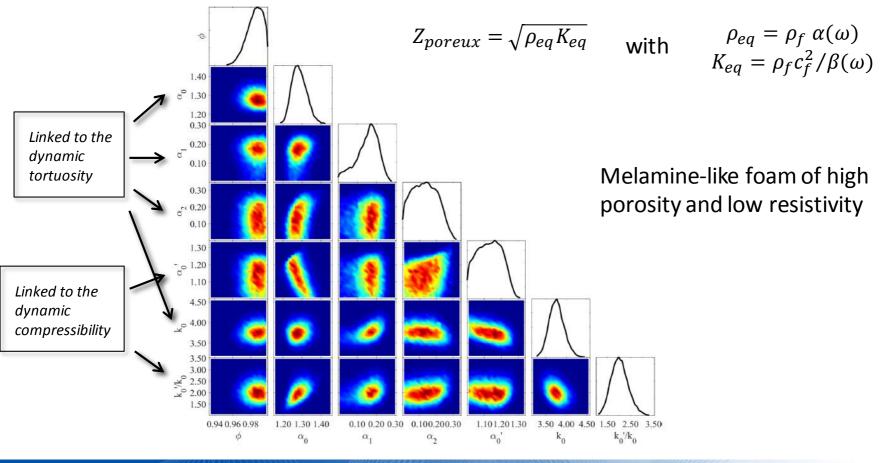


with prior knowledge



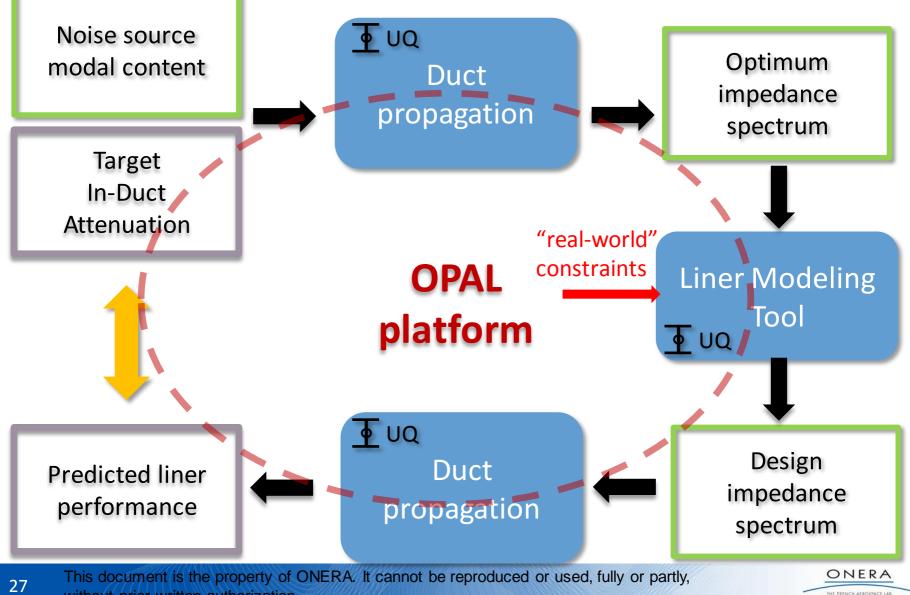
Application to porous characterization

Roncen et al. JASA vol 144 (July&Dec.) 2018; Roncen et al JASA vol 145 (March & Sep.) 2019





Liner design loop including UQ



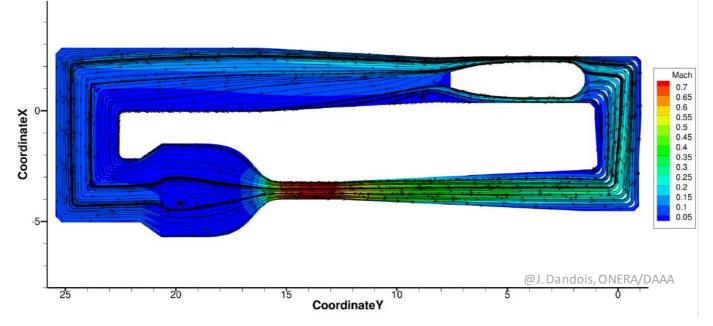
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- Context
- Liner design strategy
- Uncertainty quantification
- Illustration on recent ONERA activities





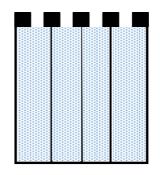


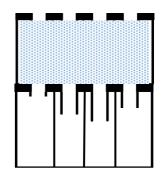
- Main challenges:
 - High-speed grazing flow (up to Mach 0,85)
 - Stringent compactness requirements
 - Mechanical resistance



Acoustic treatment of wind tunnels







Perforate + foam

Multi-Leonar

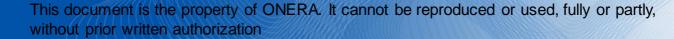
Design process

- Numerical assessment of several concepts (OPAL tool) on the target configuration (WT)
- Experimental check of the achieved impedance on a simplified configuration (Cannelle bench)
- Manufacturing and installation in the WT

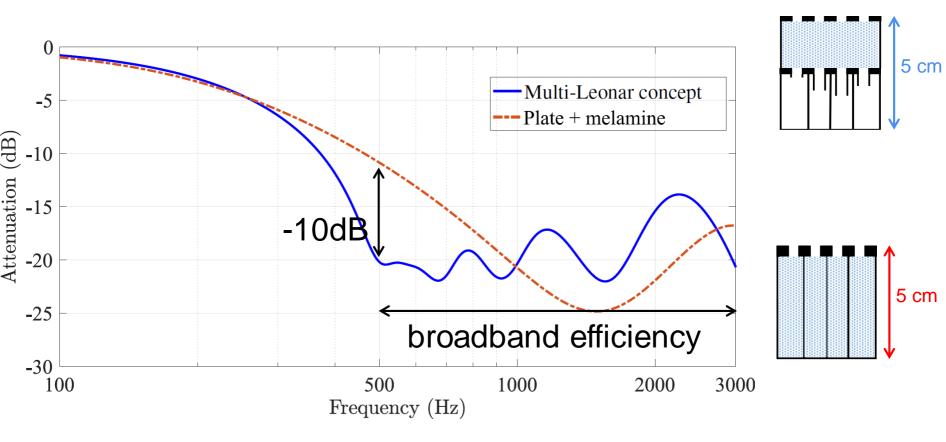


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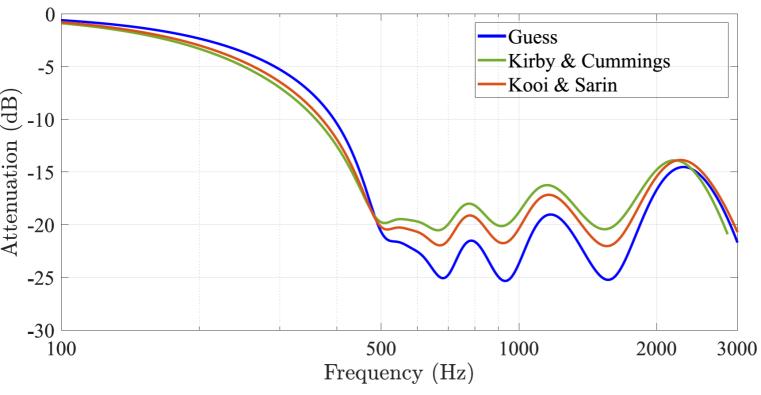


• Acoustic treatment of wind tunnels



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• Acoustic treatment of wind tunnels

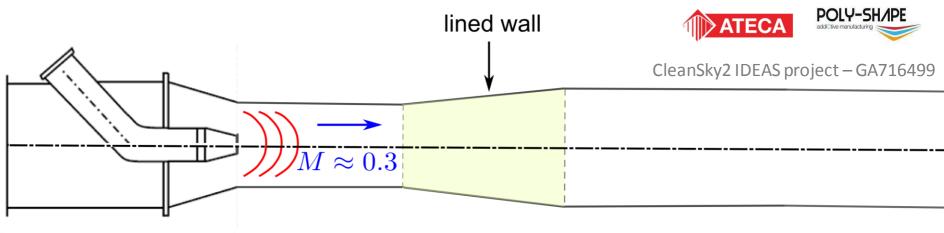


Low sensitivity of the solution to the grazing flow model (@M=0,9) → To be checked experimentally

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• Acoustic treatment of air conditioning systems

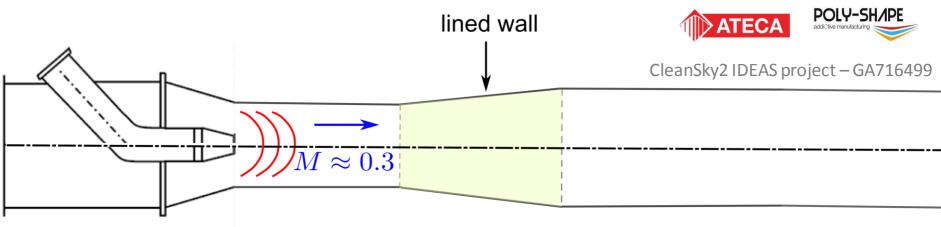


- Main challenges:
 - Stringent weight requirements
 - Temperature resistance
 - Manufacturing costs

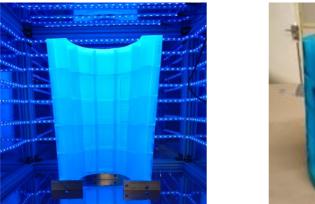


Clean Sky₂

• Acoustic treatment of air conditioning systems

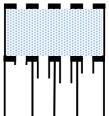


- Outcome of the design process:
 - DDOF liner with combination of foam and Leonar layers





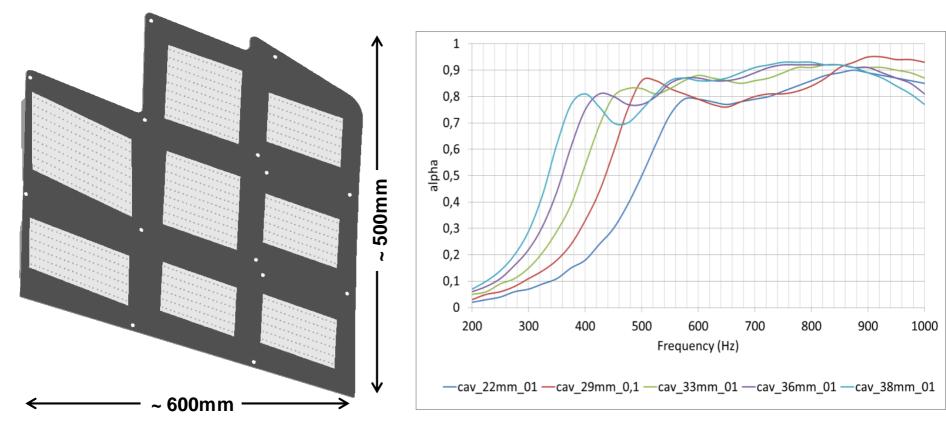




Clean Sky₂



• Broadband absorption of airframe noise



Combination of N-DOF LEONAR

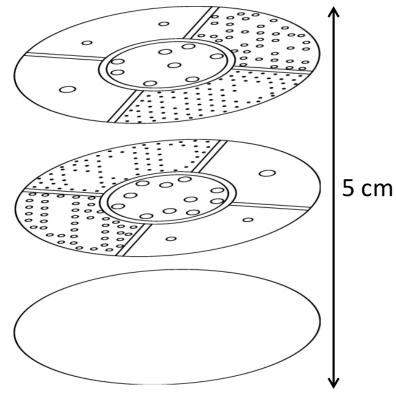
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Broadband absorption at low-frequency, with a very compact solution (~3 cm)

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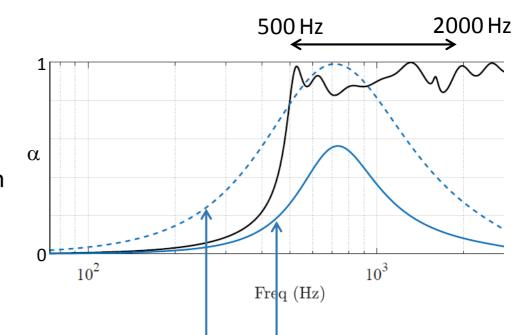
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• Low&broadband frequency liner (ONERA/TSAGI coop.)



2-DOF liner with complex perforation layout

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Perforate + honeycomb cavity at low (solid lines) and high (dashed lines) SPL

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Conclusions

- Need in the aeronautics industry of new liner solutions for noise mitigation of the innovative flying concepts
- New material technologies, especially additive manufacturing, have broadly opened the design space for liner concepts
- Manufacturing and operational constraints must be taken into account all along the liner design process
- Uncertainty quantification must be addressed to ensure robustness of the design outcome
 work in progress in the ONERA liner design platform (OPAL)



Thank you for your attention!

