

# 3D-printed Permeable Trailing Edges for Broadband Noise Abatement

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**Roma Tre University, Rome, Italy**

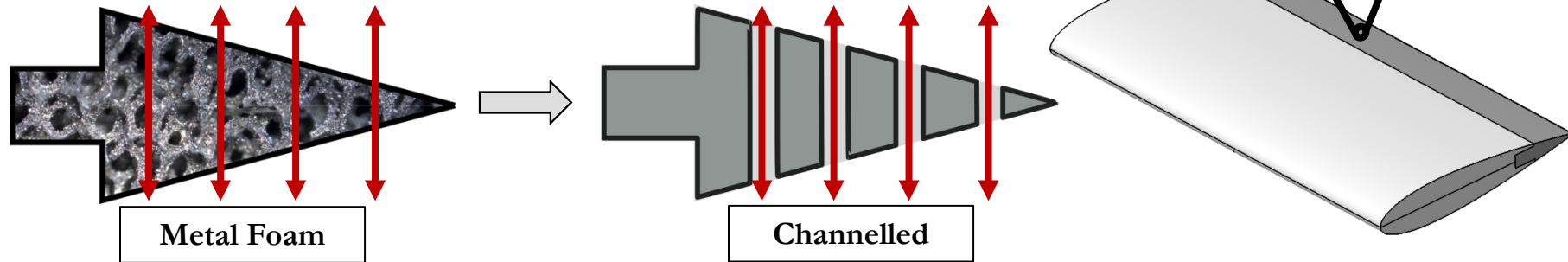
23<sup>rd</sup> Workshop of the Aeroacoustics Specialists Committee of the CEAS,  
26-27 September 2019



# Permeable Materials for Noise Reduction

- **High noise reduction** ( $\sim 11$  dB) [Rubio Carpio et al. (2018)]
- Key parameter: **Flow permeability  $K$**  [Herr et al. (2014)]
- **Decrease in lift** for larger  $K$  [Geyer et al. (2010)]
- **Partially porous airfoils**

Can we achieve similar noise attenuation effects with a parametrized pore arrangement?



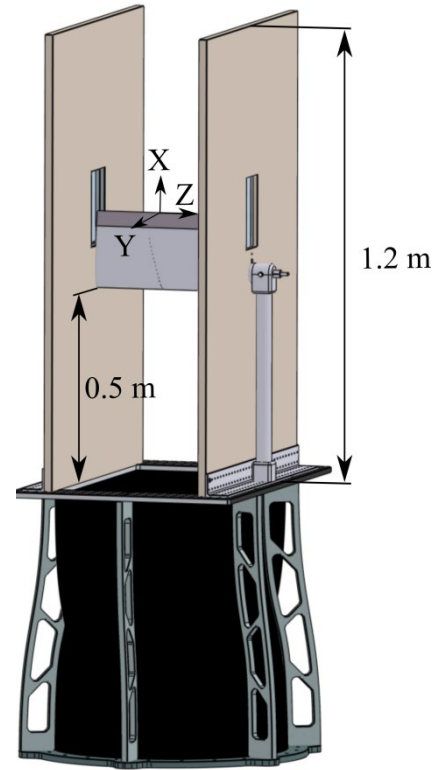
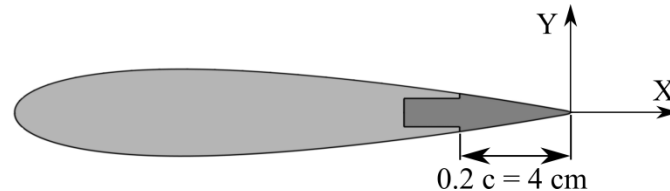
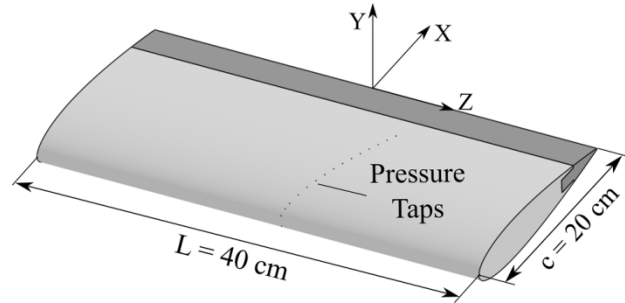
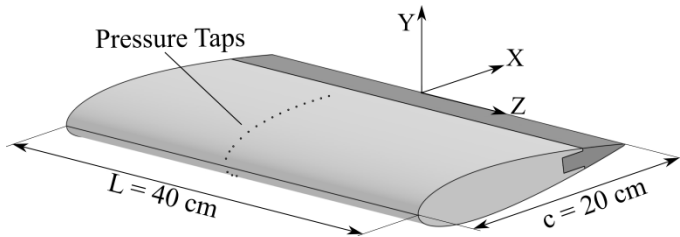
# Experimental Set-Up



# Model

- NACA 0018 airfoil:
- Exchangeable permeable inserts:
- Turbulent boundary layer transition:
- Outlet section:
- Free-stream velocity:
- $Re_c$ :
- Free-stream turbulence:

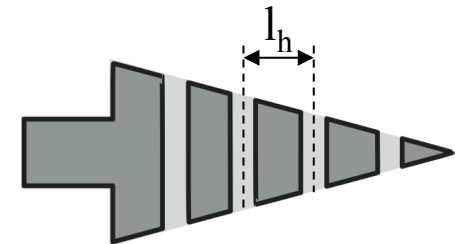
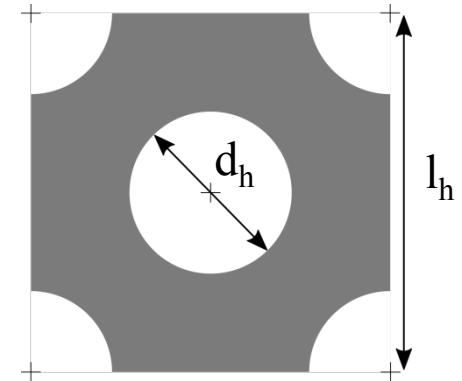
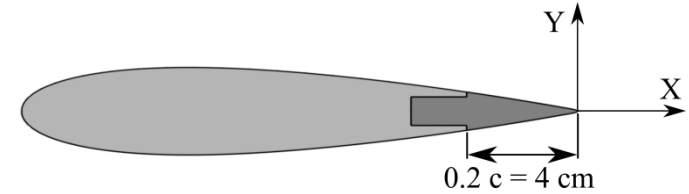
$c = 20$  cm; airfoil span:  $L = 40$  cm  
 20% of the airfoil  
 20% of the chord  
 $40 \times 70$  cm<sup>2</sup>  
 $U_\infty = 12.5 \dots 34$  m/s  
 $140,000 \dots 380,000$   
 0.05%



# 3D-printed Perforated Inserts

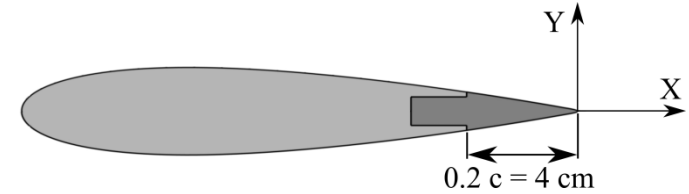
- EnvisionTEC's Perfactory 4 Standard
  - Resolution: 25  $\mu\text{m}$
  - Material: HTM 140 V2 (light-activated resin)
- Perforated inserts (x4) :
  - Span: 10 cm
  - Fixed hole diameter:  $d_h = 0.8 \text{ mm}$
  - Varying hole spacing:  $l_h = 1.5, \dots, 5 \text{ mm}$

$$l_h = 1.5 \text{ mm}$$



# 3D-printed Perforated Inserts

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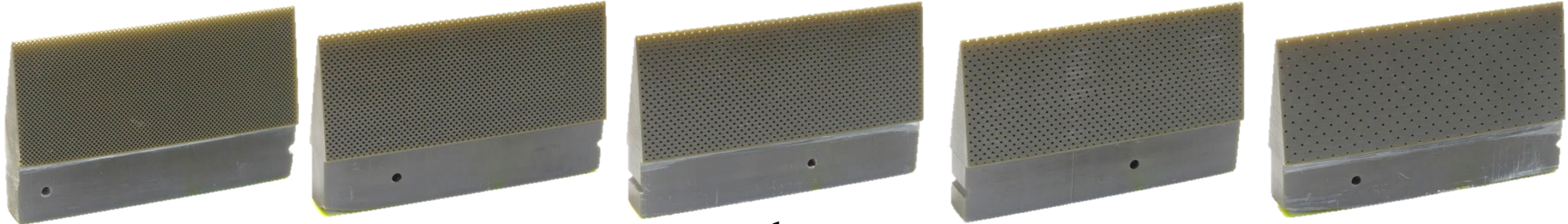
$l_h = 1.5 \text{ mm}$

$l_h = 2.0 \text{ mm}$

$l_h = 2.5 \text{ mm}$

$l_h = 3.0 \text{ mm}$

$l_h = 5.0 \text{ mm}$



$l_h$

$K$

# Permeability Characterization

- Perforated samples:
  - $t = 1$  cm; diameter of 5.5 cm
  - $l_h = 1.5, \dots, 6$  mm

## Hazen-Dupuit-Darcy Law:

$$\frac{\Delta p}{t} = \frac{\mu}{K} v_d + \rho C v_d^2 \quad [\text{Ingham (1998)}]$$

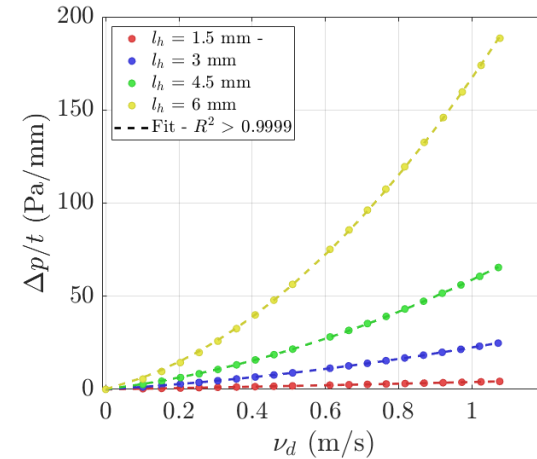
$\Delta p$ : pressure drop across the metal foam sample (Pa)

$\mu$ : dynamic viscosity (Pa s)

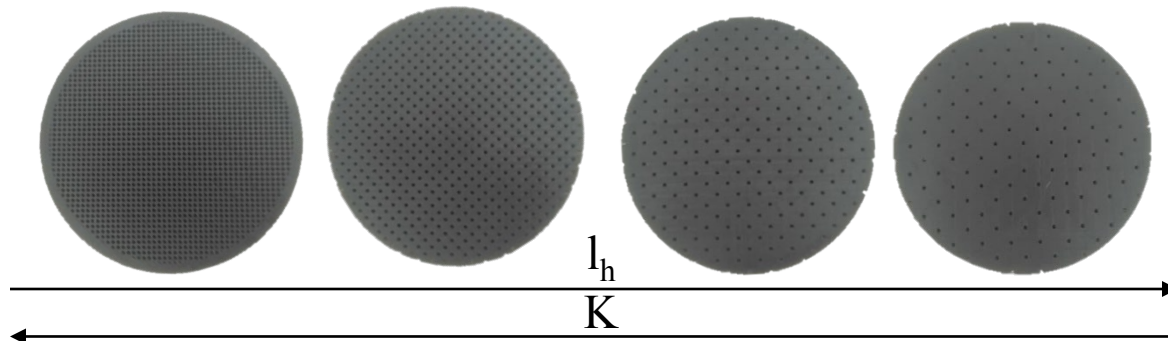
$\rho$ : density (kg/m<sup>3</sup>)

$v_d$ : velocity (m/s)

$t$ : thickness of the sample (m)



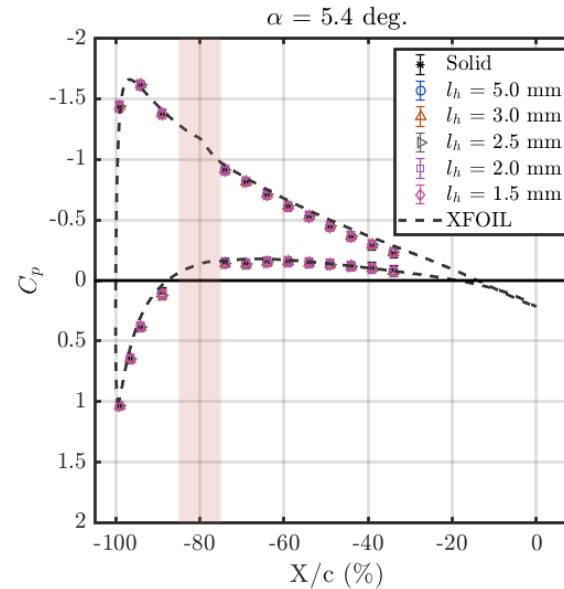
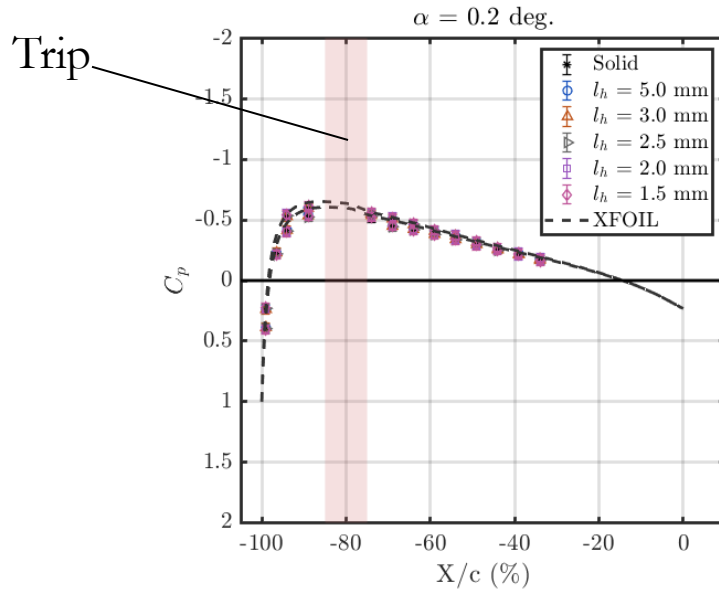
$l_h$ (mm)	$K$ (m <sup>2</sup> ) ( $\times 10^{10}$ )
1.5	50
2	28
2.5	18
3	13
5	5



# Experimental Set-up

- Honeywell TruStability pressure sensors:
- Wind tunnel angle of attack:
- Effective angle of attack:

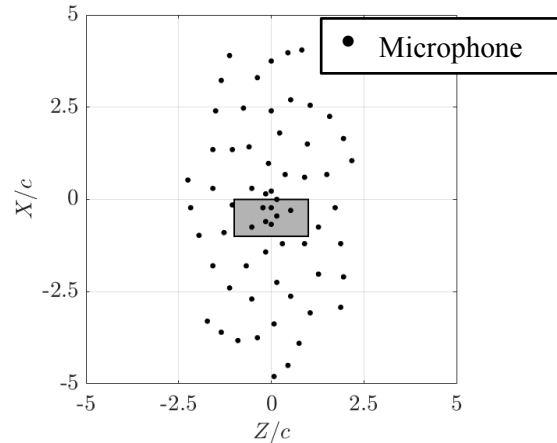
range: -2.5 to 2.5 kPa; accuracy:  $\pm 0.25\%$  FS  
 $\alpha_t = 0$  and 8 deg.  
 $\alpha = 0.2$  and 5.4 deg. (XFOIL)



- No change in measured pressure distribution due to perforated inserts

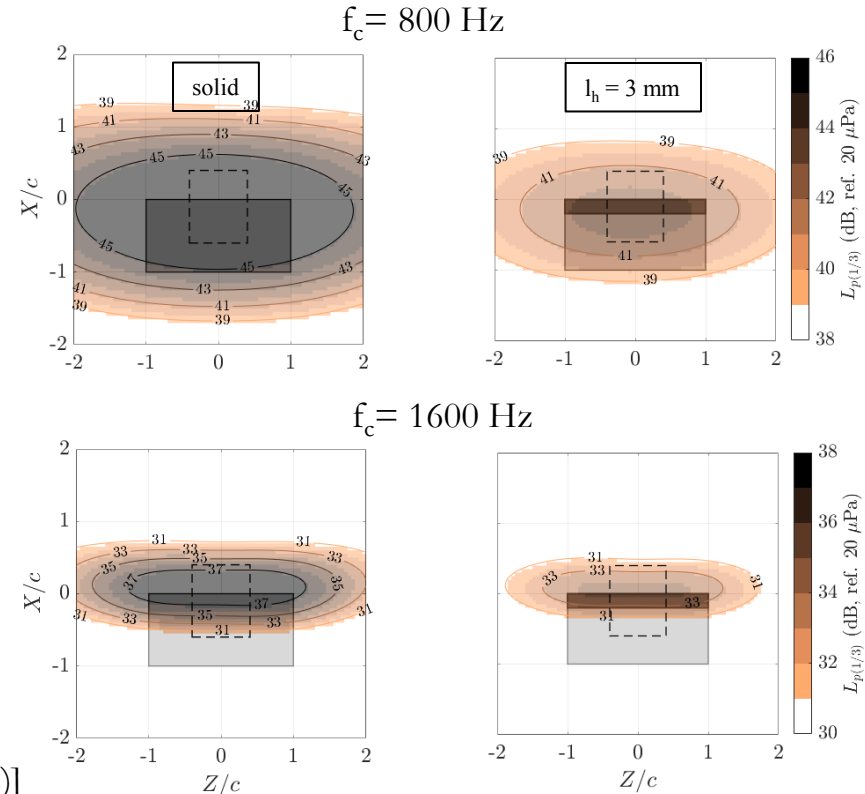


# Experimental Set-up

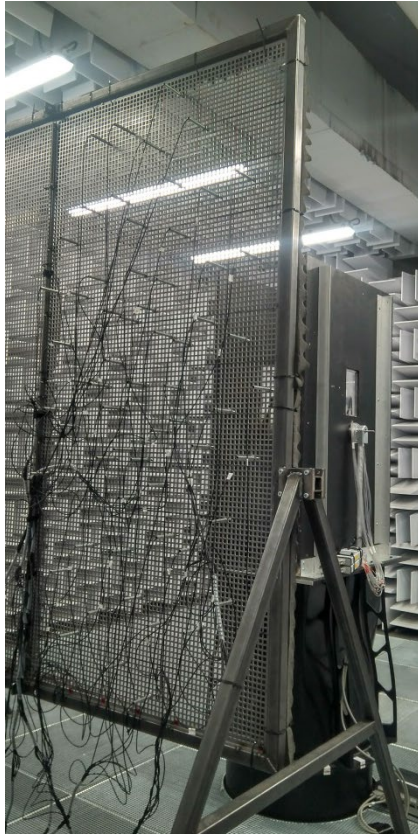


## Hardware, acquisition parameters & data-processing:

- (64x) G.R.A.S. 40PH. free-field microphones:  $D = 2$  m
- Distance array-trailing edge:  $1$  m
- Acquisition frequency:  $f_s = 50$  kHz
- Acquisition period:  $T = 20$  s
- Acoustic camera looking at suction side
- Adapted Underbrink design [Underbrink (2001)]
- Conventional frequency domain beamforming [Mueller (2002)]
- Source Power Integration [Sarradj et al. (2017)]



# A-Tunnel



# Results & Discussion

# Results

## Broadband Noise Abatement with Channelled Inserts

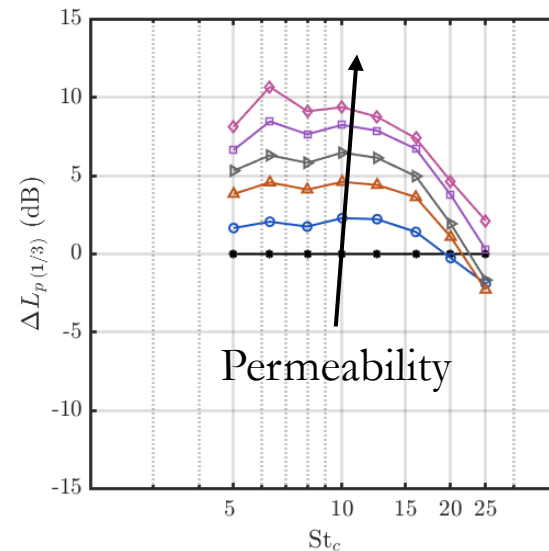
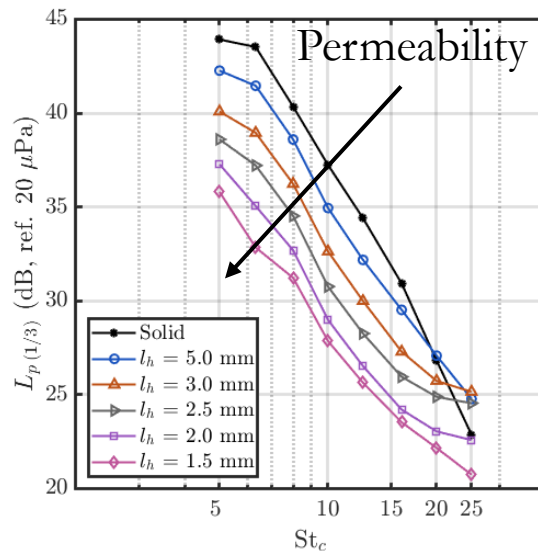
- Sound Pressure Level at approximately no incidence,  $U = 20$  m/s

$\alpha = 0.2$  deg.

$$St_c = \frac{f c}{U_\infty}$$

$$L_p = 10 \log_{10} \frac{\overline{p^2}}{p_0^2}$$

p: far-field ac. pressure (Pa)  
 $p_0$ : reference pressure (Pa)  
 f: frequency (Hz)  
 $U_\infty$ : free-stream velocity (m/s)  
 c: chord (m)



# Results

## Broadband Noise Abatement with Channelled Inserts

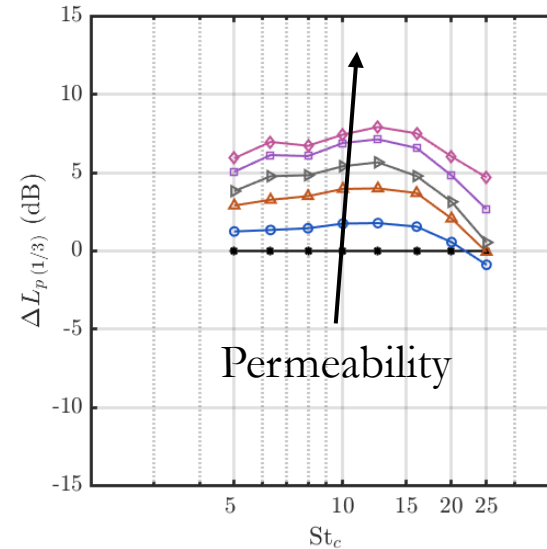
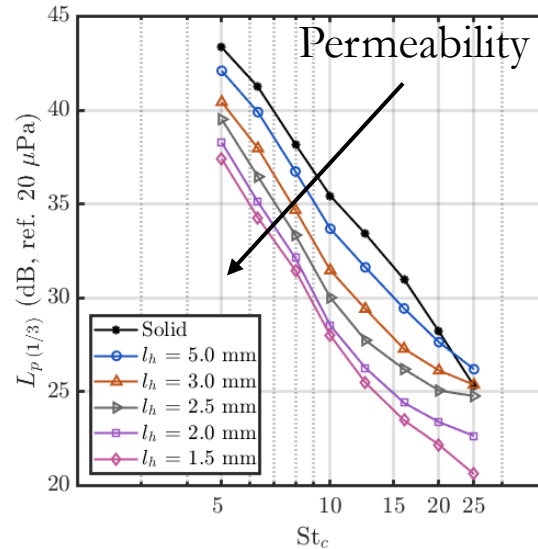
- Sound Pressure Level at a lifting condition,  $U = 20$  m/s

$\alpha = 5.4$  deg.

$$St_c = \frac{f c}{U_\infty}$$

$$L_p = 10 \log_{10} \frac{\overline{p^2}}{p_0^2}$$

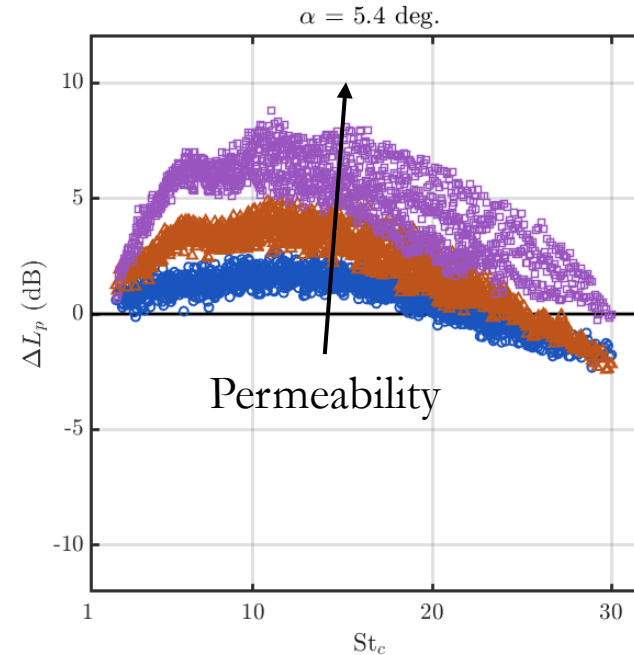
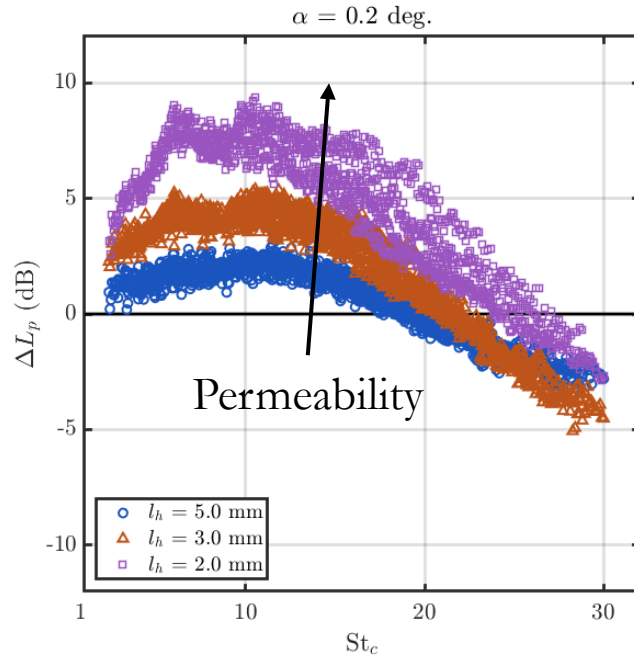
$p$ : far-field ac. pressure (Pa)  
 $p_0$ : reference pressure (Pa)  
 $f$ : frequency (Hz)  
 $U_\infty$ : free-stream velocity (m/s)  
 $c$ : chord (m)



# Results

## Broadband Noise Abatement with Channelled Inserts

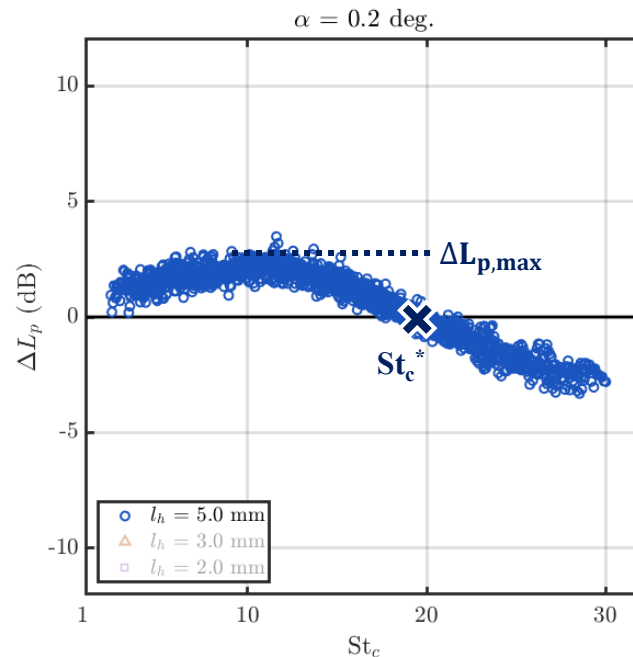
- Collapse of noise attenuation data measured at  $U_\infty = 12.5, 15, 20, 25, 30, 34$  m/s with a simple Strouhal number relationship



# Results

## Broadband Noise Abatement with Channelled Inserts

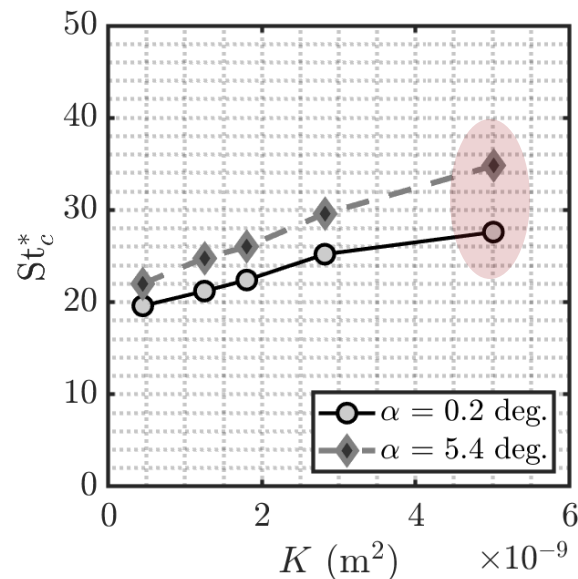
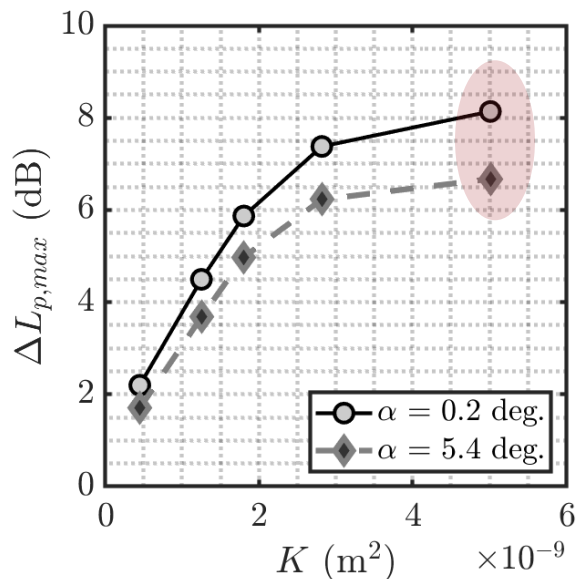
- Collapse of noise attenuation data measured at  $U_\infty = 12.5, 15, 20, 25, 30, 34$  m/s with a simple Strouhal number relationship
- Computation of maximum noise reduction  $\Delta L_{p,\max}$  and cross-over Strouhal number  $St_c^*$



# Results

## Broadband Noise Abatement with Channelled Inserts

- Variation of maximum noise reduction  $\Delta L_{p,max}$  and cross-over Strouhal number  $St_c^*$  with permeability  $K$ .

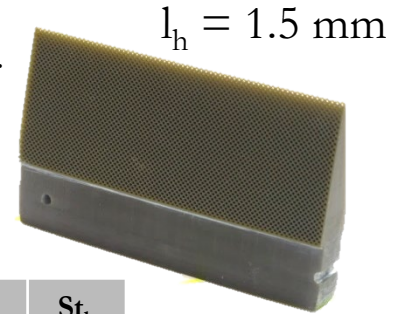
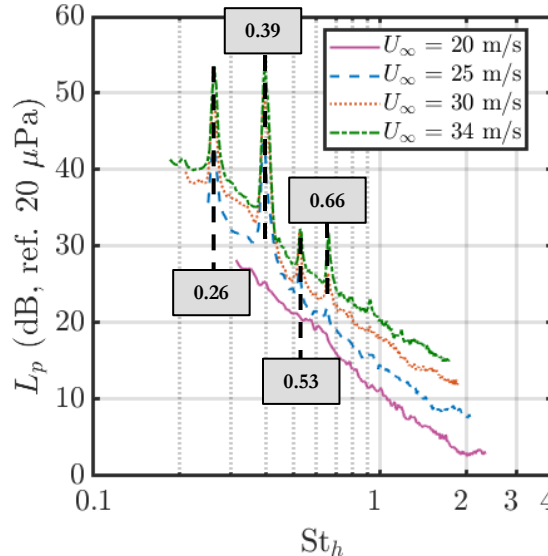
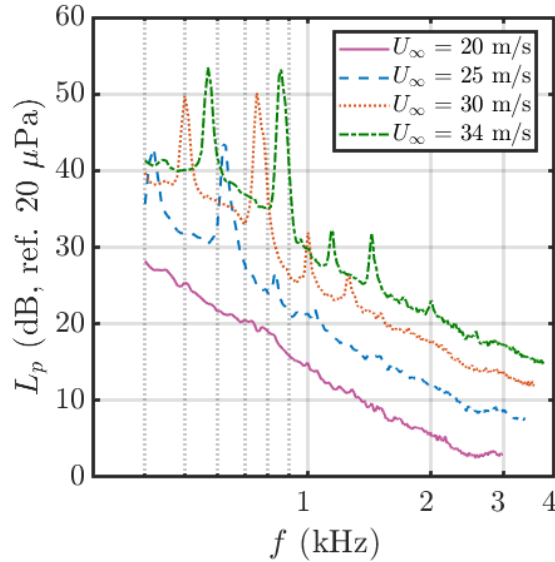




# Results

## Tonal Noise at Channelled Inserts

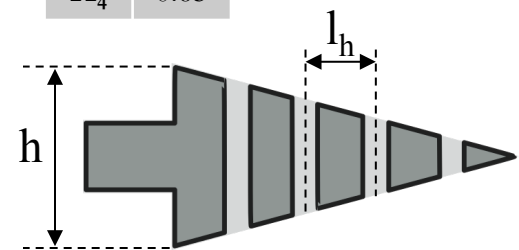
- Appearance of tonal noise for the most permeable perforated insert ( $l_h = 1.5$  mm).



	$St_h$
<b>FT</b>	<u>0.13</u>
$H_1$	0.26
$H_2$	0.39
$H_3$	0.52
$H_4$	0.65

$$St_h = \frac{f h}{U_\infty}$$

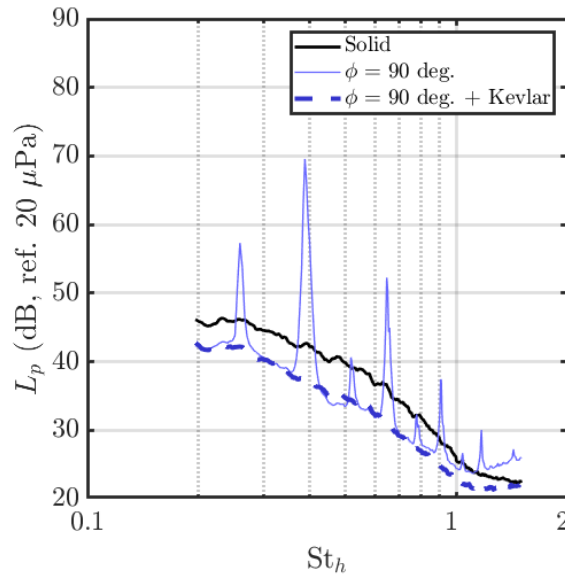
- Strouhal number based on the airfoil thickness at the root of the insert ( $h = 15.7$  mm) for the fundamental tone ( $= 0.13$ ) is in line with airfoil blunt trailing-edge noise ( $\sim 0.11$ ).



# Results

## Tonal Noise at Channelled Inserts

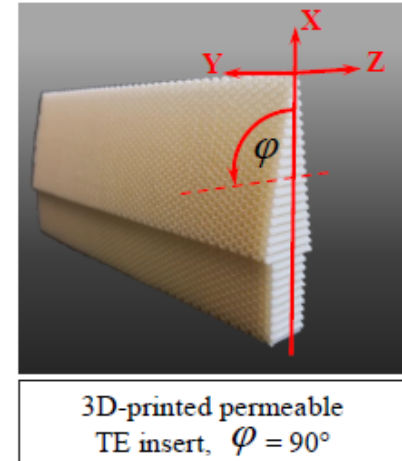
- Another way is to cover the inserts with Kevlar.
- Far-field acoustic spectra for  $\alpha = 0$  deg. and  $U_\infty = 40$  m/s



Material	$d_h$ (mm)	$K$ (m <sup>2</sup> ) (x10 <sup>10</sup> )
HTM 140 V2	0.8	50
PLA	1.2	233
PLA + Kevlar*	1.2	72

\*Kevlar 49T965 fabric, weight-to-area ratio of 61 g/m<sup>2</sup>, density of 1,45 g/m<sup>3</sup>, thickness of 0,12 mm.

	$St_h$
FT	0.13
H <sub>1</sub>	0.26
H <sub>2</sub>	0.39
H <sub>3</sub>	0.52
H <sub>4</sub>	0.65
H <sub>5</sub>	0.78
H <sub>6</sub>	0.91



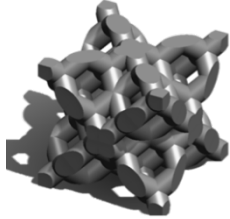
[S. Luesutthiviboon et al. (2019), Int. Jour. Aeroac., submitted]

# Preliminary Results

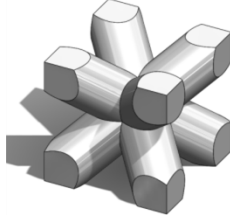
## 3D-Printed Porous Media

- Far-field acoustic spectra for  $\alpha = 0$  deg. and  $U_\infty = 40$  m/s

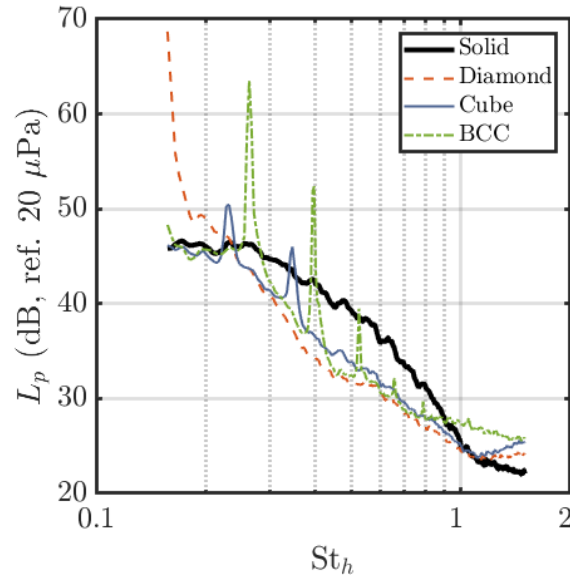
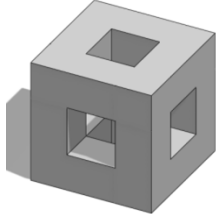
Diamond



BCC



Cubic



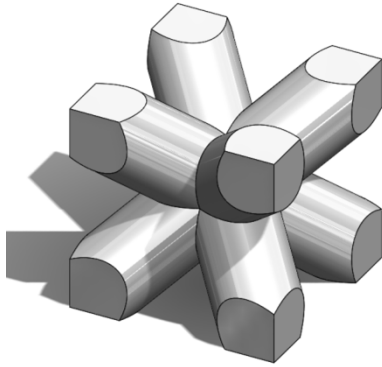
Material	Shape	$K(\text{m}^2)$ ( $\times 10^{10}$ )
HTM 140 V2	Channelled	50
PLA	Diamond	160
PLA	BCC	153
PLA	Cube	158

	$St_h$		
	Diamond	Cube	BCC
FT	<u>0.15</u>	<u>0.12</u>	<u>0.13</u>
$H_1$	-	0.23	0.26
$H_2$	-	0.35	0.39
$H_3$	-	0.47	0.53

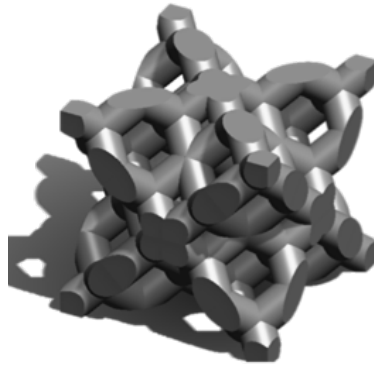
[R. Hedayati et al. (2020)]

# Ongoing Work

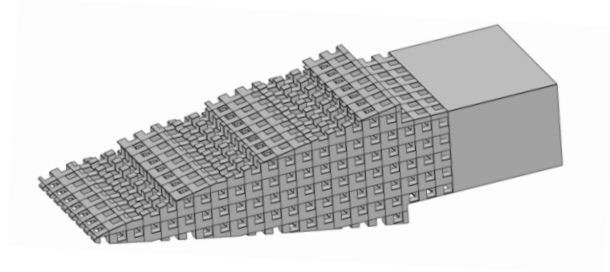
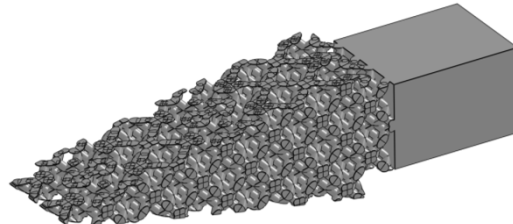
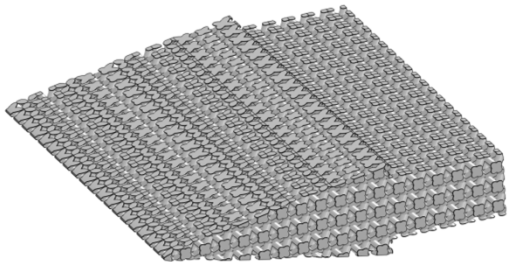
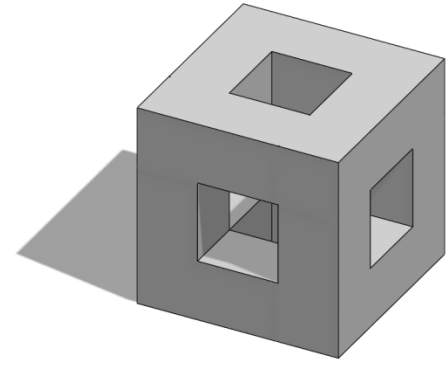
BCC



Diamond



Cubic



[R. Hedayati et al. (2020)]

# Conclusions

# Conclusions

- Perforated inserts mimic the behaviour of other permeable treatments with more complex micro-structure.
- Perforated inserts yield up to 11 dB noise attenuation at  $\alpha = 0.2$  deg., and up to 9 dB at  $\alpha = 5.4$  deg. for increasing flow permeability.
- Noise attenuation w.r.t. the baseline configuration collapses with a simple chord-based Strouhal number relationship.
- The maximum noise attenuation and the cross-over Strouhal number can be empirically correlated to the permeability.
- For inserts with very high permeability, a tonal noise appears at a Strouhal number based on the thickness of the solid-permeable junction ranging from 0.13 to 0.15; the exact value depends on the pore arrangement.
- The tonal noise can be modified by employing treatments with a streamwise permeability gradient or by covering the inserts with Kevlar.

# References

- *A. Rubio Carpio, F. Avallone, D. Ragni*; **On the Role of the Flow Permeability of Metal Foams on Trailing Edge Noise Reduction**; 24th AIAA/CEAS Aeroacoustics Conference; AIAA 2018-2964; <https://doi.org/10.2514/6.2018-2964>
- *A. Rubio Carpio, R. Merino Martinez, F. Avallone, D. Ragni, M. Snellen, S. van der Zwaag*; **Experimental characterization of the turbulent boundary layer over a porous trailing edge for noise abatement**; Journal of Sound & Vibration 443 (2019) 537-558; <https://doi.org/10.1016/j.jsv.2018.12.010>
- *A. Rubio Carpio, F. Avallone, D. Ragni, M. Snellen, S. van der Zwaag*; **3D-printed Perforated Trailing Edges for Broadband Noise Abatement**; 25th AIAA/CEAS Aeroacoustics Conference; AIAA 2019-2458; <https://doi.org/10.2514/6.2019-2458>
- *J. Meyer, A. Rubio Carpio, D. Ragni*; **Temperature-Activated Change of Permeable Material Properties for Low-Noise Trailing Edge Applications**; Applied Sciences (2019) 9, 3119; <https://doi.org/10.3390/app9153119>
- *S. Luesutthiviboon, D. Ragni, F. Avallone, M. Snellen*; **Aeroacoustics Investigation of an Airfoil with Kevlar-covered 3D-printed Permeable Trailing Edge**; International Journal of Aeroacoustics; Submitted
- *A. Rubio Carpio, F. Avallone, D. Ragni, M. Snellen, S. van der Zwaag*; **Mechanisms of Broadband Noise Generation on Metal Foam Edges**; Physics of Fluids; Accepted for Publication
- *A. Rubio Carpio, F. Avallone, D. Ragni, M. Snellen, S. van der Zwaag*; **3D-printed Permeable Trailing Edges for Broadband Noise Abatement**; AIAA Journal; To be submitted

**Thank you for your attention!**





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