

Smart Mitigation of flow-induced Acoustic Radiation and  
Transmission for reduced Aircraft, Surface traNSport,  
Workplaces and wind enERgy noise



## Trailing Edge Noise Reduction with Permeable Materials:

## Description of Noise Scattering Mechanism



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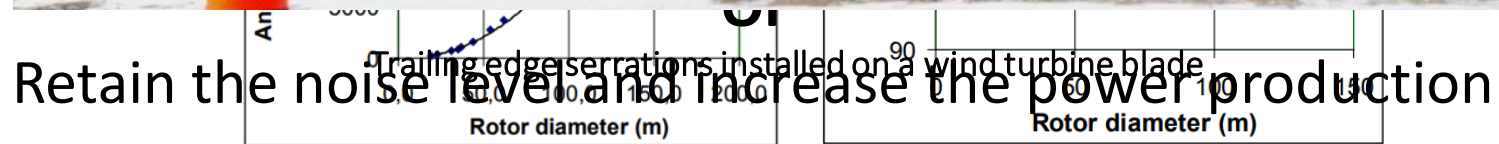
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# I. INTRODUCTION



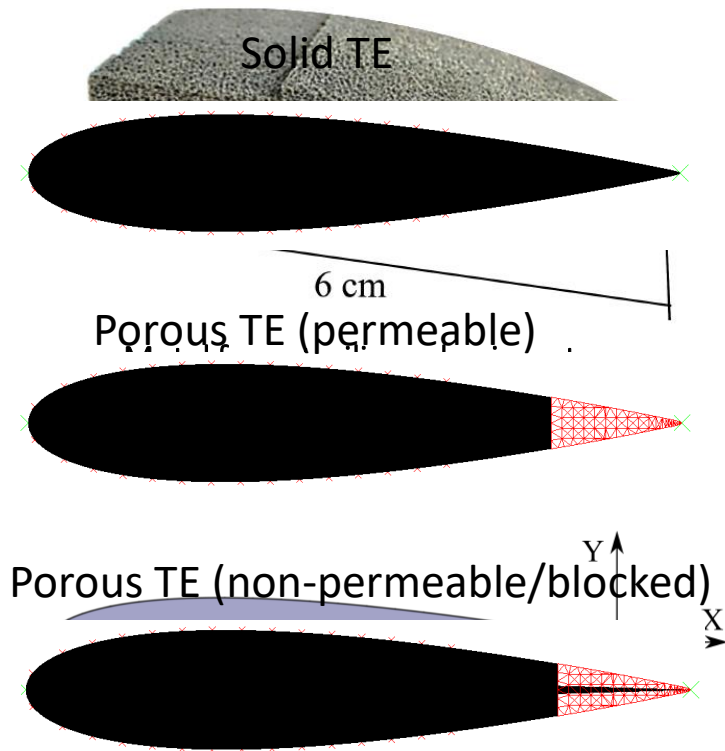
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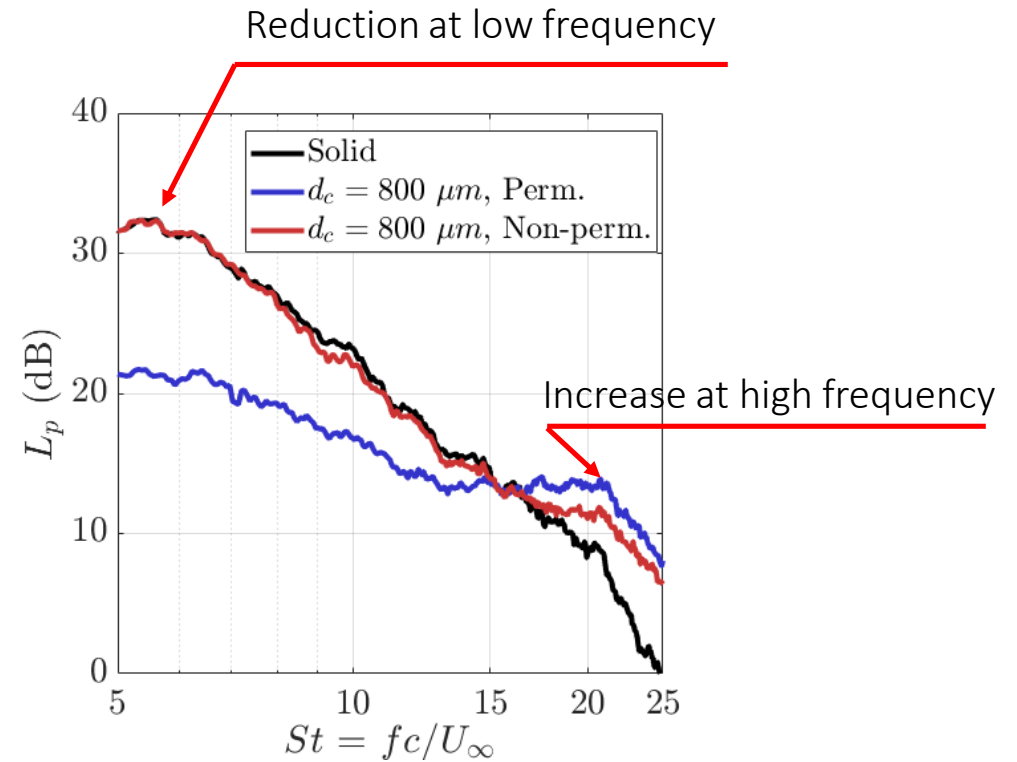
[1] <http://www.windenergy.org.nz/improvements-in-technology>

[2] <http://www.ewea.org/events/workshops/wp-content/uploads/2012/12/EWEA-Noise-Workshop-Oxford-2012-1-1-Stefan-Oerlemans.pdf>

[3] <http://www.windfarmbop.com/serrations-or-how-to-reduce-those-noisy-vortexes/>



NACA 0018 with metal-foam trailing edge [1]  
Different types of trailing edge treatment

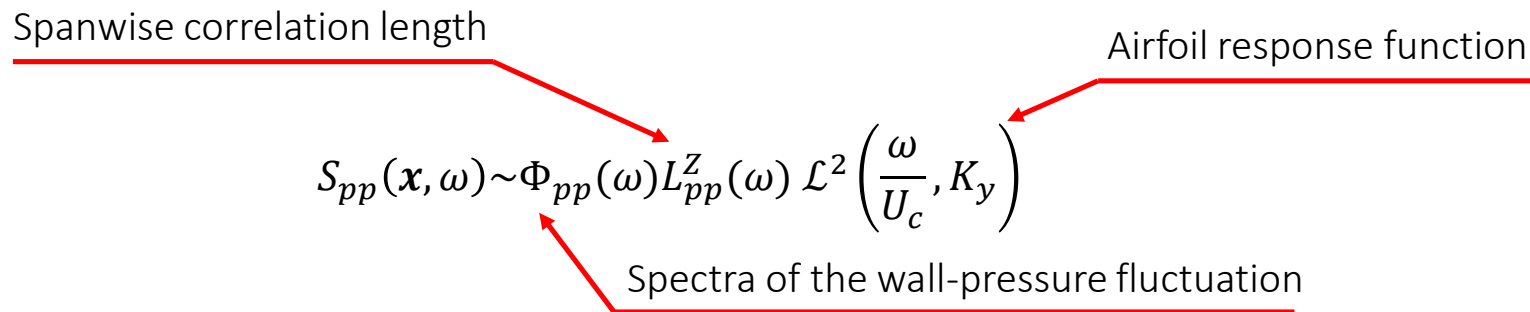


Far field sound spectra comparison [1]

[1] Rubio Carpio *et al.*, "On the role of the flow permeability of metal foams on trailing edge noise reduction", 2018 AIAA/CEAS Aeroacoustics Conference

[2] Rubio Carpio *et al.*, "Mechanisms of Broadband Noise Generation on Metal Foam Edges", *Physics of Fluids*, under review.

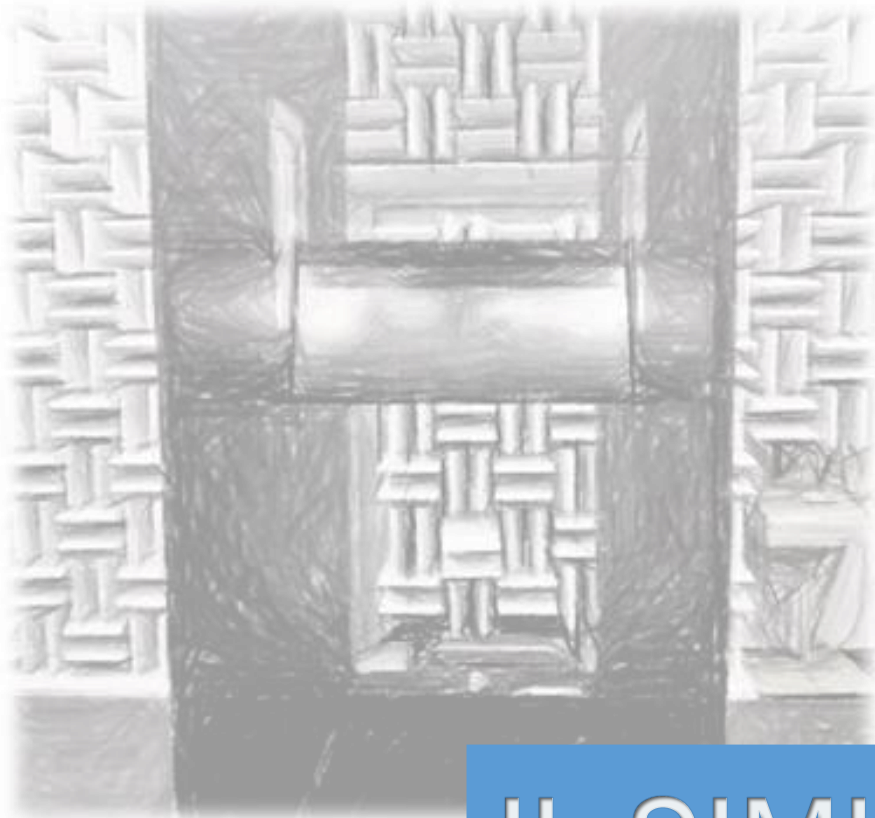
- Trailing-edge permeability affects noise reduction, but how?
- Some parameters that are proportional to far-field noise according to Amiet's model [1,2] :



- Could the changes in these parameters be linked to the noise reduction?
- To gain more insights into the aeroacoustics of porous trailing edge, a numerical study is performed using **PowerFLOW 5.4b**.

[1] Amiet, R. K, Noise due to turbulent flow past a trailing edge. *Journal of sound and vibration*, 47(3), 387-393, 1976

[2] Roger, M., & Moreau, S., Back-scattering correction and further extensions of Amiet's trailing-edge noise model. Part 1: theory. *Journal of Sound and Vibration*, 286(3), 477-506, 2005

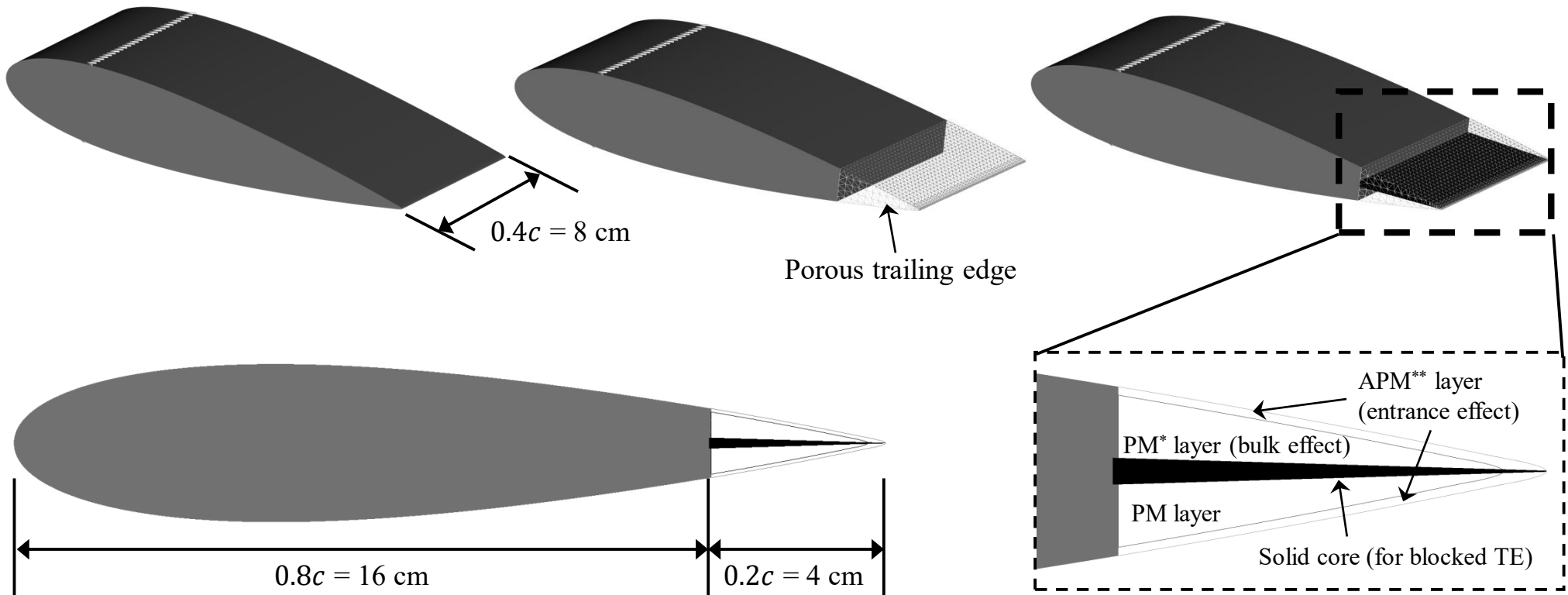


## II. SIMULATION AND RESULTS

(a) Solid TE

(b) Porous TE

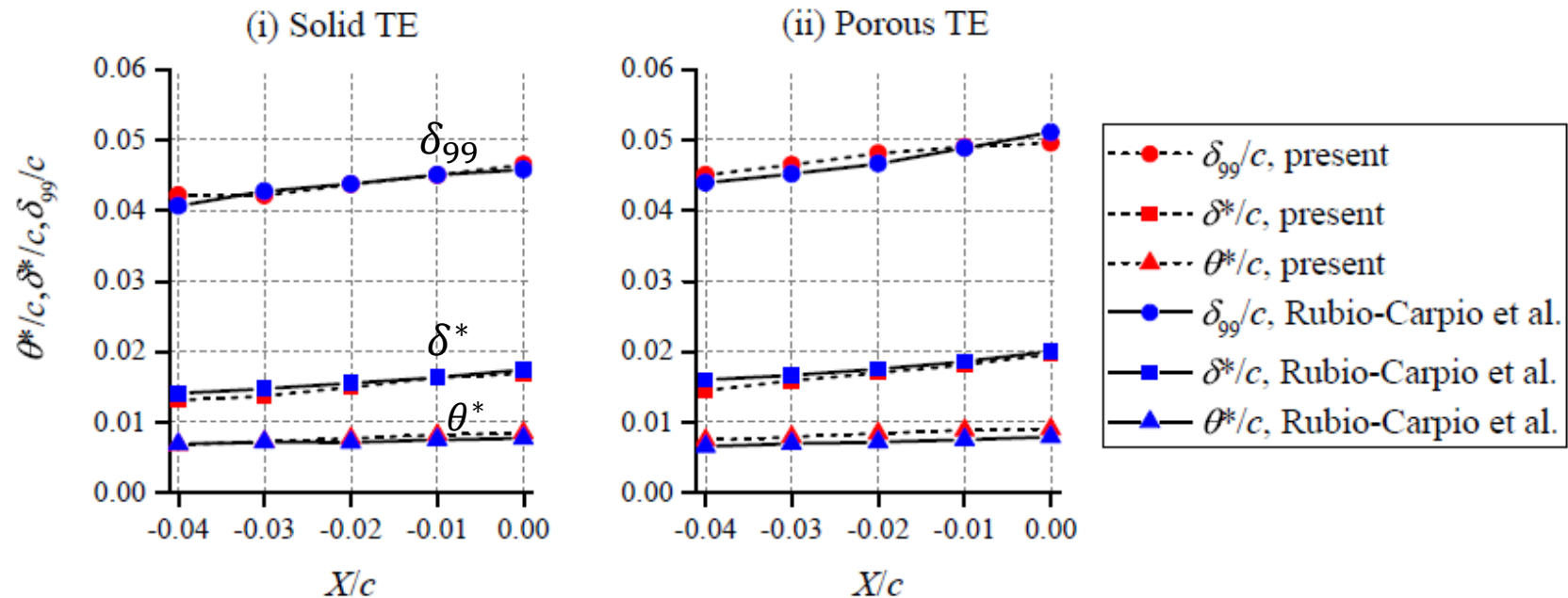
(c) Blocked TE



- The porous material is modelled using equivalent fluid regions governed by Darcy's law.

\* PM (Porous Material) – an equivalent fluid region where certain mechanical impedance can be specified, subjecting the permeating fluid to viscous and inertial losses.

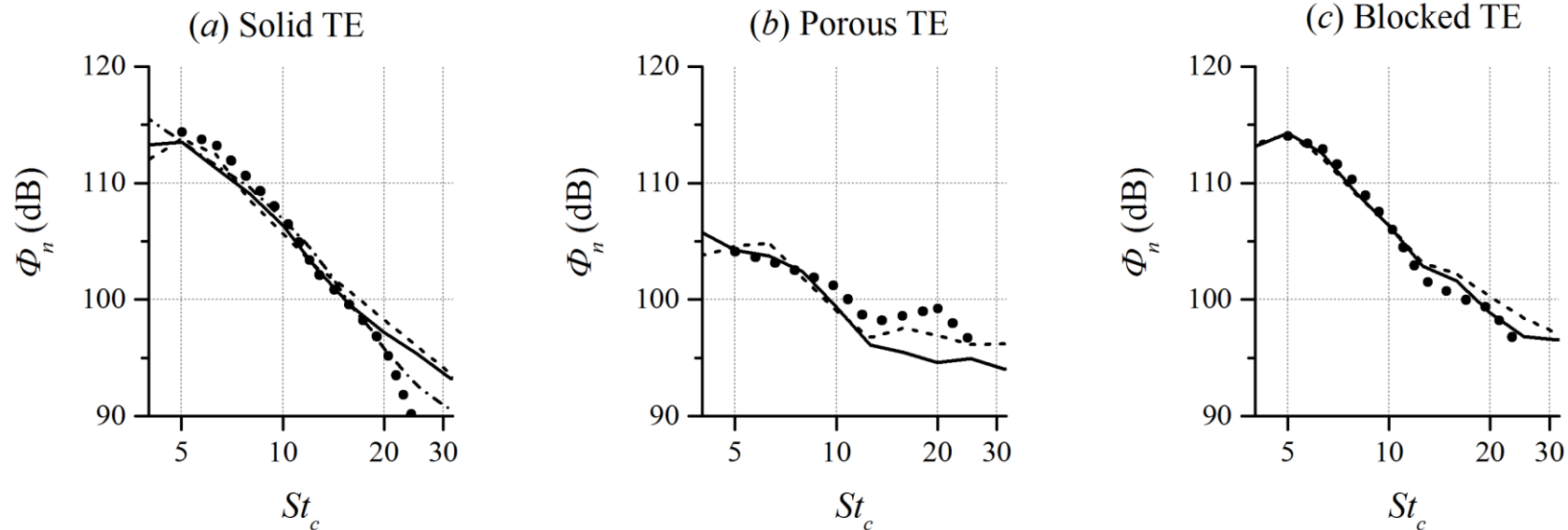
\*\* APM (Acoustics Porous Material) – a model similar to the PM with the addition of porosity, which governs the mass flow of transpiration across the porous medium surface



Comparison of boundary layer integral parameters between the simulation and the experiment

[1] Carpio, A. R., Martínez, R. M., Avallone, F., Ragni, D., Snellen, M., & Van Der Zwaag, S. Broadband trailing edge noise reduction using permeable metal foams. In *46th International Congress and Exposition of Noise Control Engineering* (pp. 27-30), 2017.





$$\Phi_n = \Phi_o + 10 \log_{10} \frac{R^2}{bM_\infty^5}$$

$$St_c = \frac{fc}{U_\infty}$$

— Surface FW-H, Present  
 - - - - Permeable FW-H, Present

•••• Rubio-Carpio et al. (2018)  
 - - - - Arce-Leon et al. (2016)

Far-field sound spectra from the three trailing edge treatments

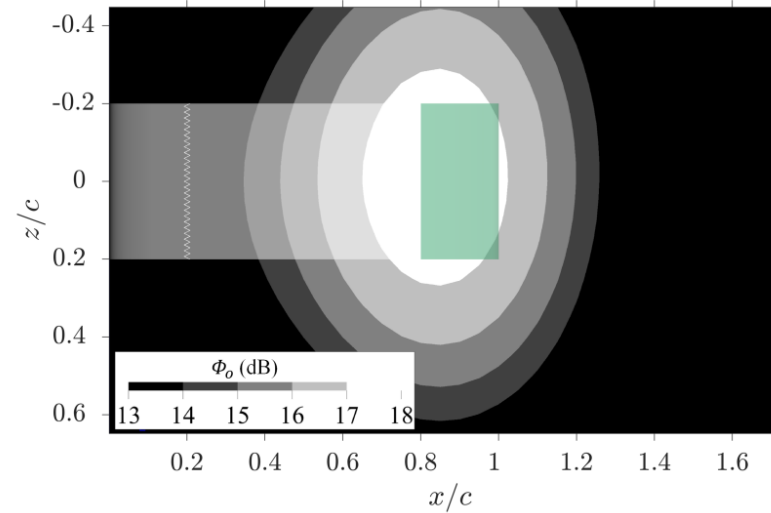
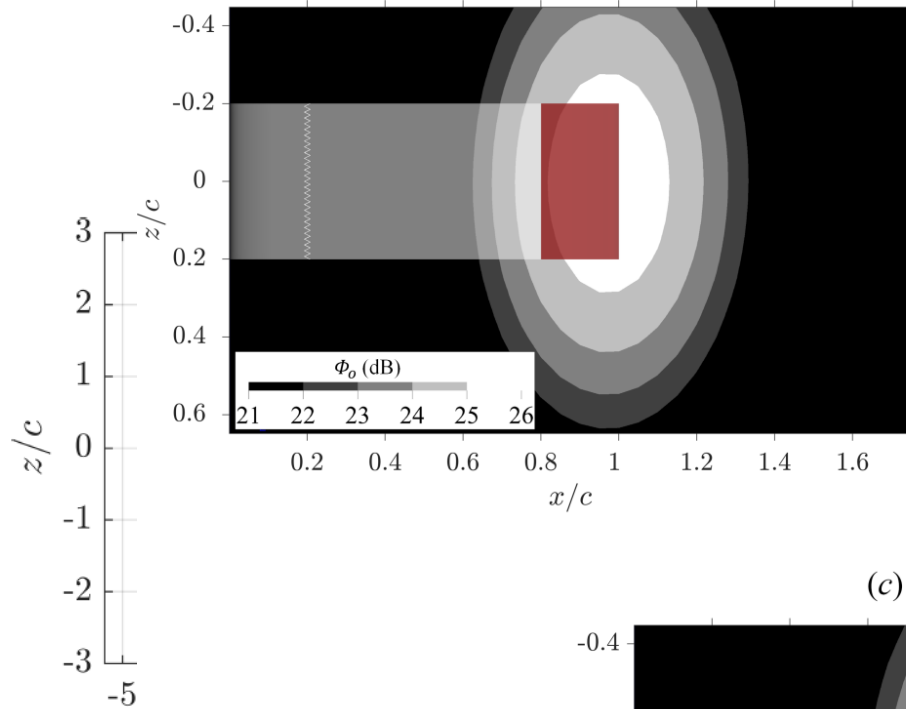
- There are discrepancies, mainly in the high frequency, however simulation results remain in trend with the experiment.

[1] Rubio Carpio *et al.*, “On the role of the flow permeability of metal foams on trailing edge noise reduction”, *2018 AIAA/CEAS Aeroacoustics Conference*

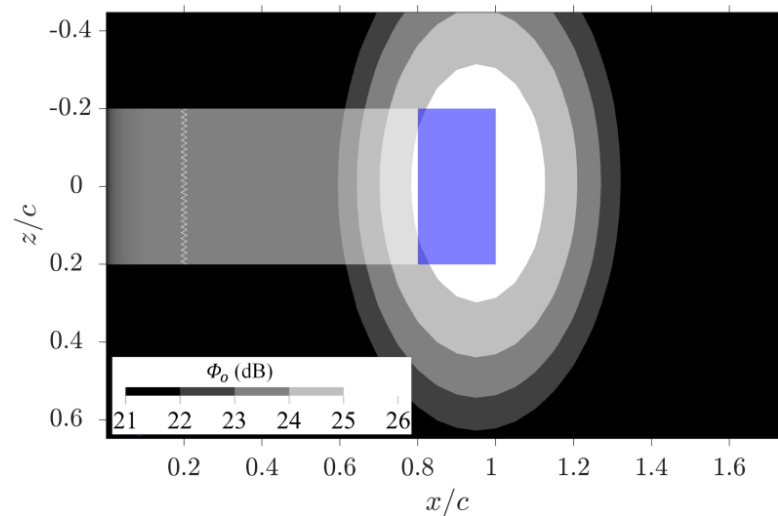
[2] León, C. A., Merino-Martínez, R., Ragni, D., Avallone, F., & Snellen, M., Boundary layer characterization and acoustic measurements of flow-aligned trailing edge serrations. *Experiments in Fluids*, 57(12), 182, 2016.

(a) Solid TE

(b) Porous TE



(c) Blocked TE



Tunnel

Beamforming maps at  $St_c = 12.5$

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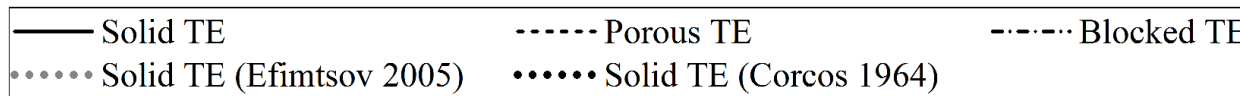
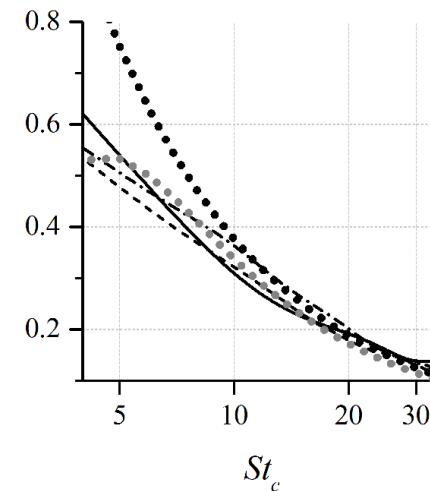
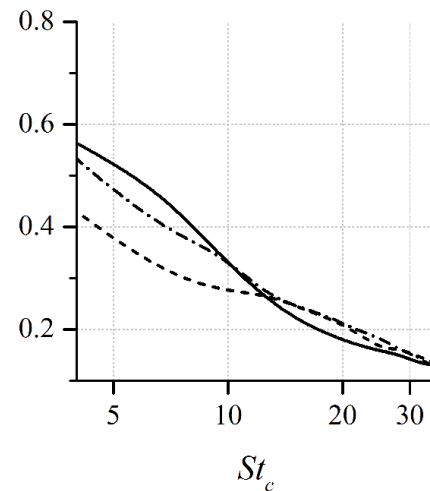
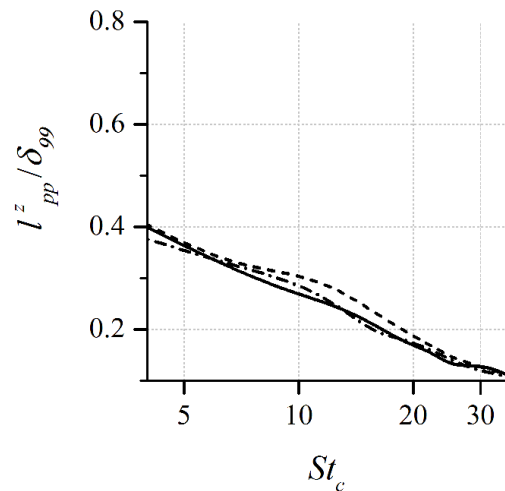


$$S_{pp}(x, \omega) \sim \Phi_{pp}(\omega) L_{pp}^Z(\omega) \mathcal{L}^2\left(\frac{\omega}{U_c}, K_y\right)$$

(a)  $x/c = -0.23$

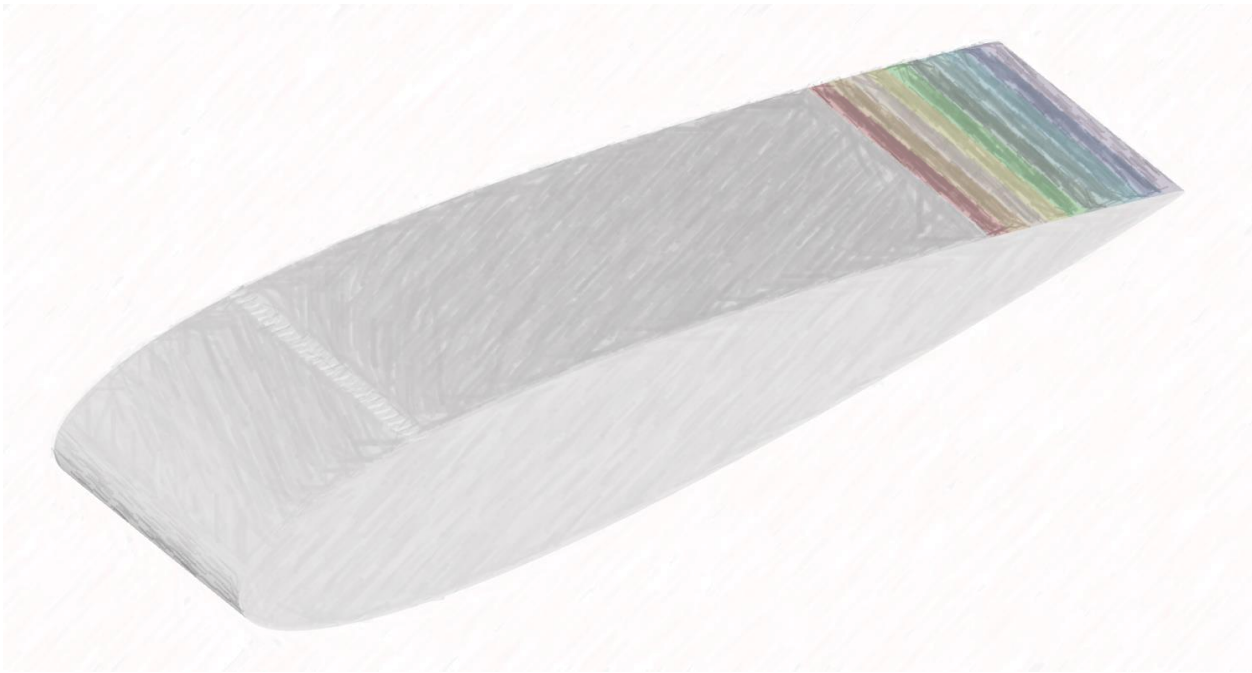
(b)  $x/c = -0.11$

(c)  $x/c = -0.01$

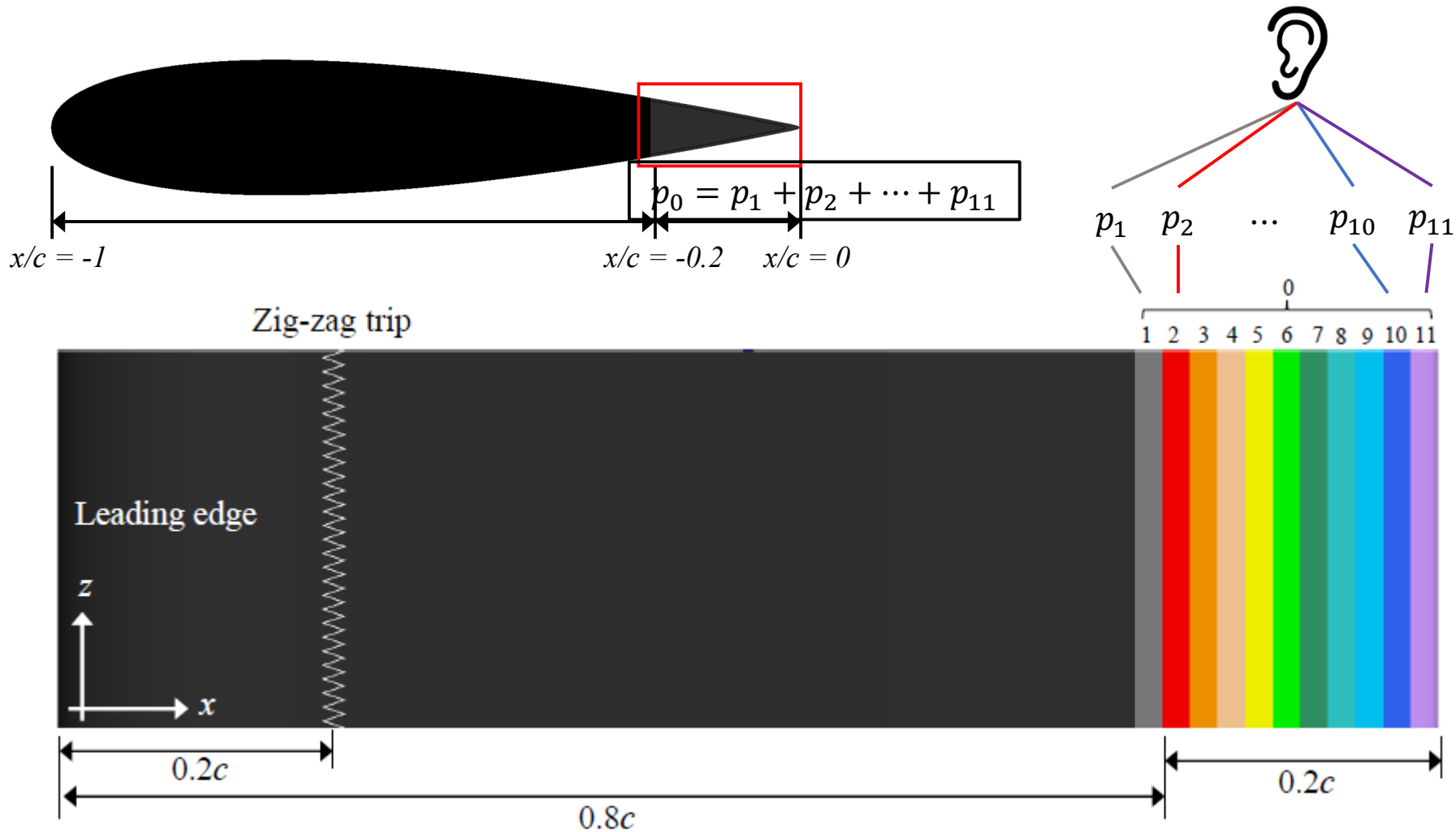


Autospectrum of surface pressure fluctuation

- The changes in the surface pressure statistics do not warrant the noise reduction of the porous TE.



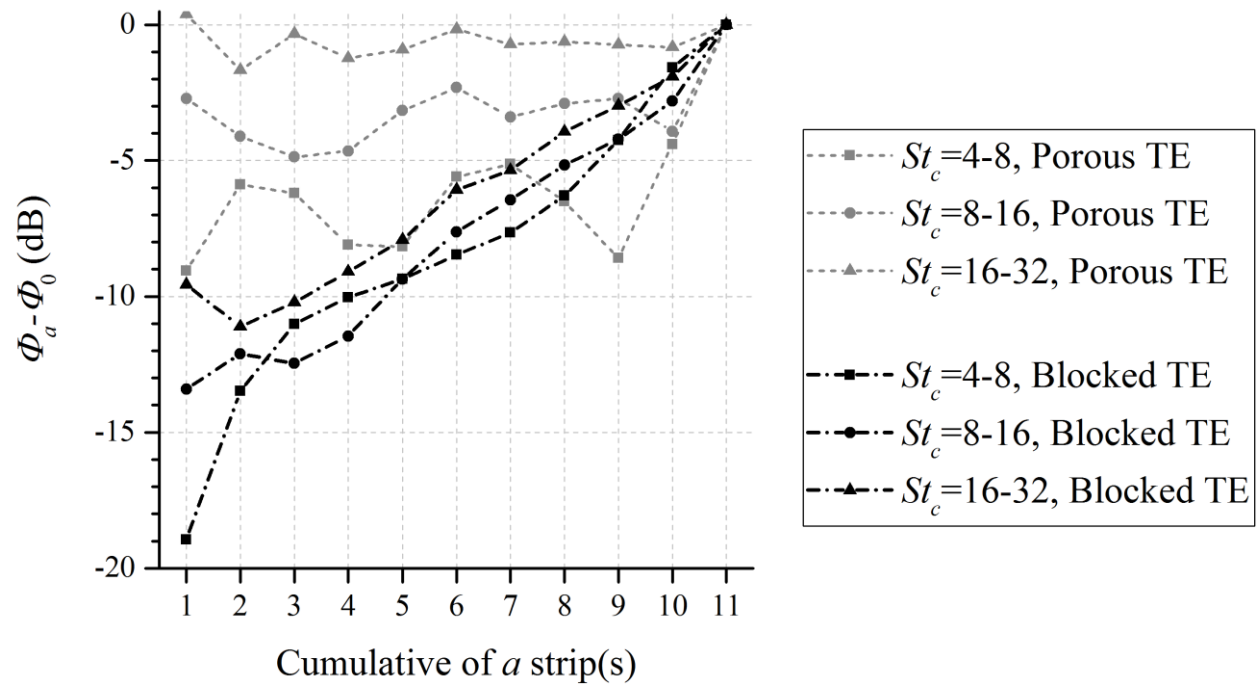
## IV. ACOUSTIC SCATTERING ANALYSES



- The trailing edge is sub-divided into strips to quantify their far-field noise contributions.

$$\Phi_a = \Phi(p_1 + \dots + p_a)$$

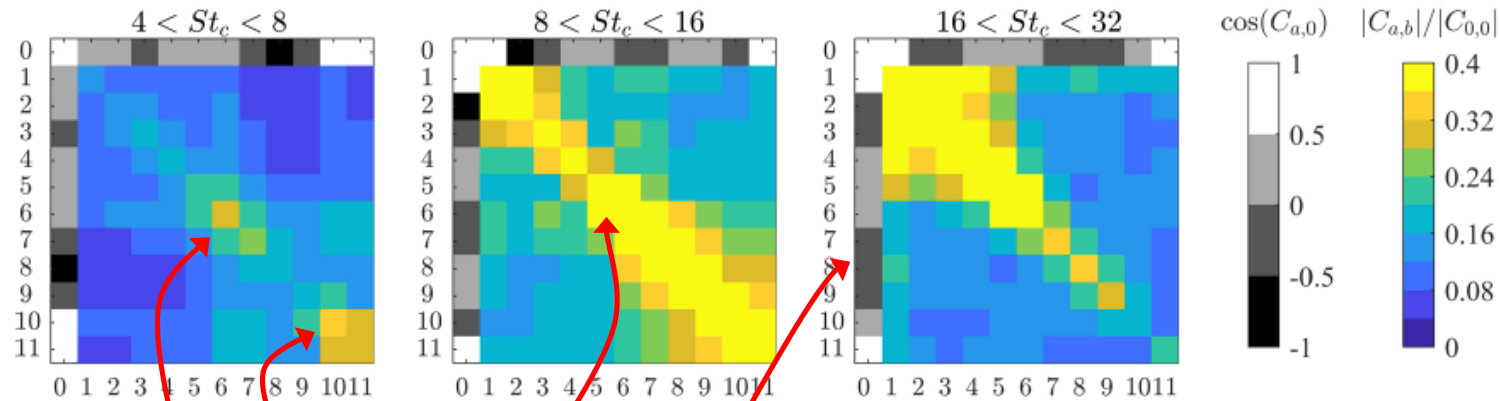
$$\Phi_0 = \Phi(p_1 + \dots + p_{11})$$



Cumulative far-field noise contribution of strips

- Strip 1 and 2 of the porous TE (i.e., solid-porous junction) have more dominant contributions than those of the blocked TE.
- Porous TE shows a large variation of slope, indicating the presence of destructive interference.

(a) Porous trailing edge



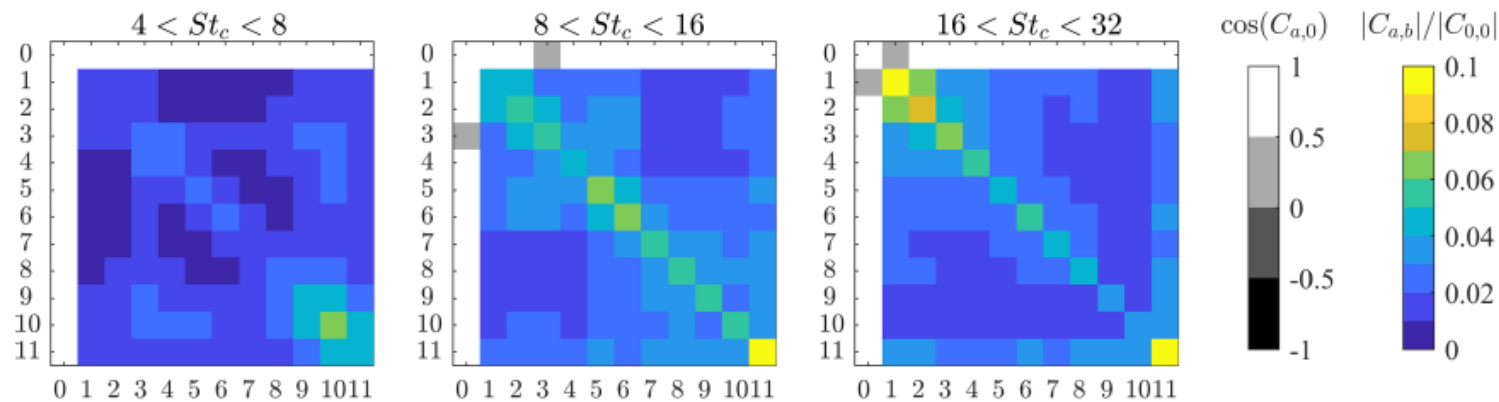
1. More uniform distribution of sound sources

2. More numbers of strips with out-of-phase relationship

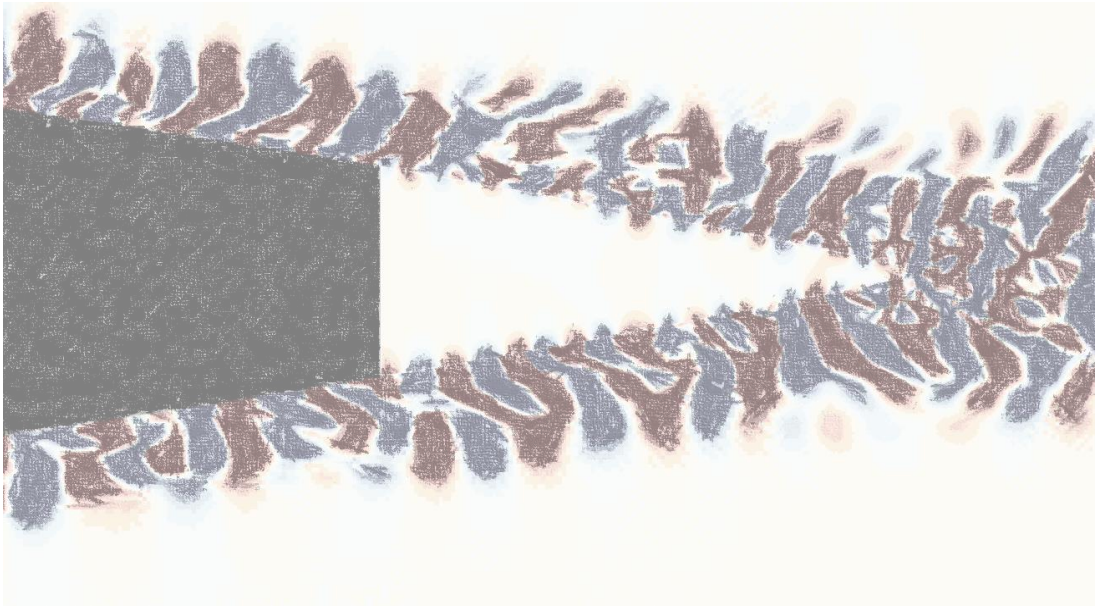
Phase angle between strip  $a$  and 0

CPSD of strip  $a$  and  $b$  normalized with autospectrum of strip 0

(b) Blocked trailing edge



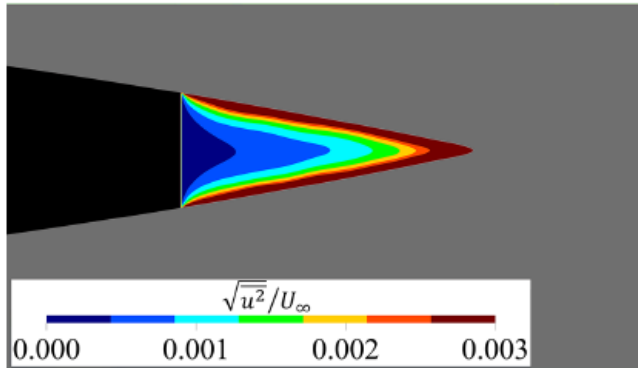
Cross-power spectral density (CPSD) matrix between strips for different TE treatments



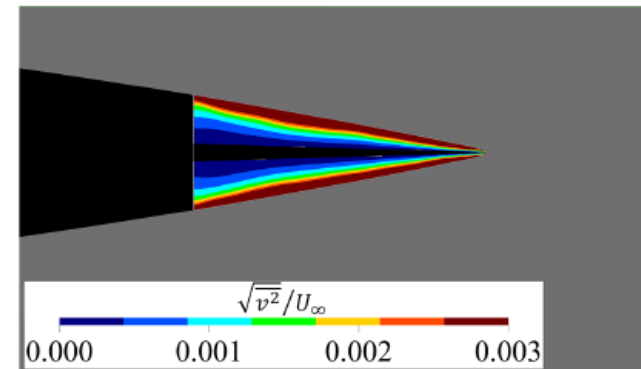
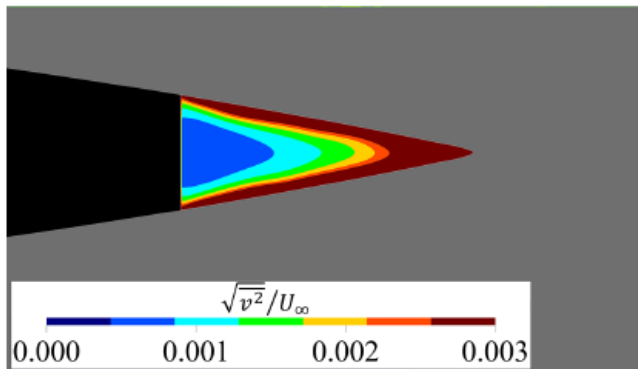
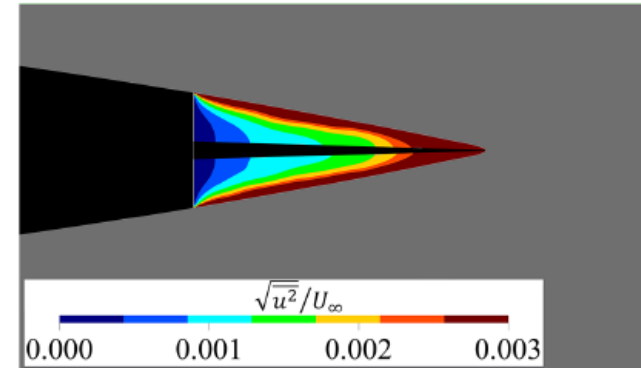
## V. THE EFFECTS OF PERMEABILITY



(a) Porous TE



(b) Blocked TE



Contours of mean freestream parallel and freestream normal velocity fluctuations

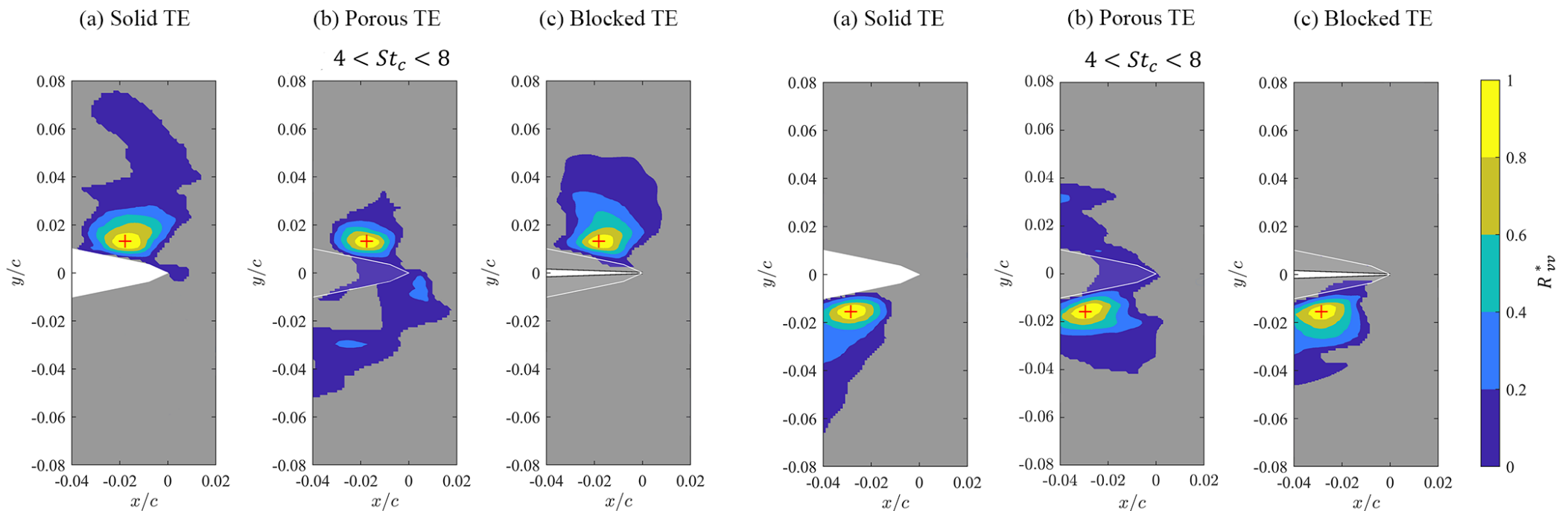
- The contours show weak recirculating flow-field inside the porous medium.
- Nevertheless, the freestream-normal velocity fluctuations are quite different between both cases.

- The permeability of the porous TE might allow the flow-field from both sides of the airfoil to “communicate” through the porous medium.

- The correlation of the wall-normal velocity  $R_{vv}^*$  is defined as: 
$$R_{vv}^*(x, x + \Delta x) = \frac{\overline{v(x)v(x+\Delta x)}}{v(x)^2}$$

(i)  $x/c = -0.018$

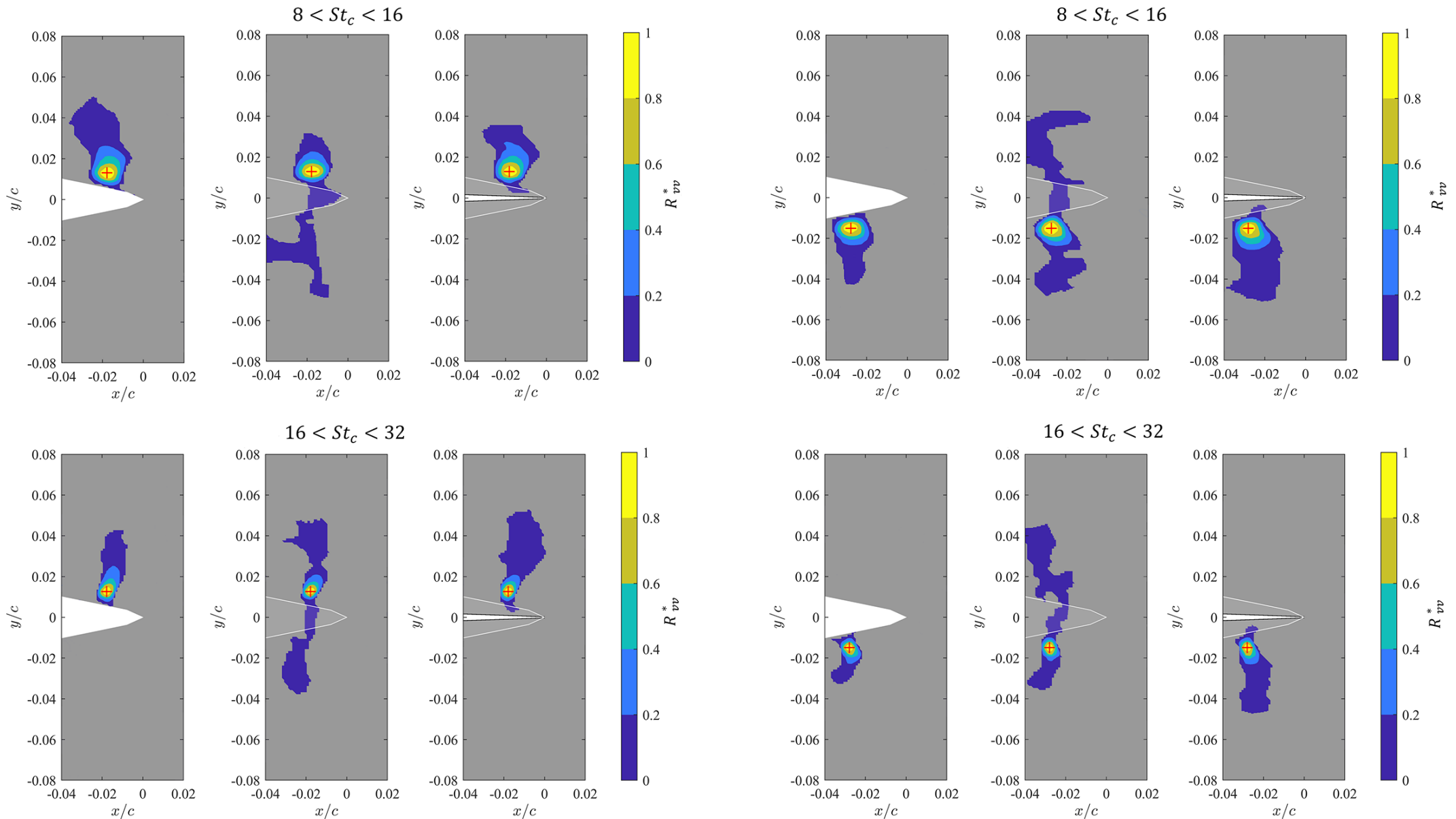
(ii)  $x/c = -0.028$



Cross-correlation of wall-normal velocity fluctuations

(i)  $x/c = -0.018$

(ii)  $x/c = -0.028$

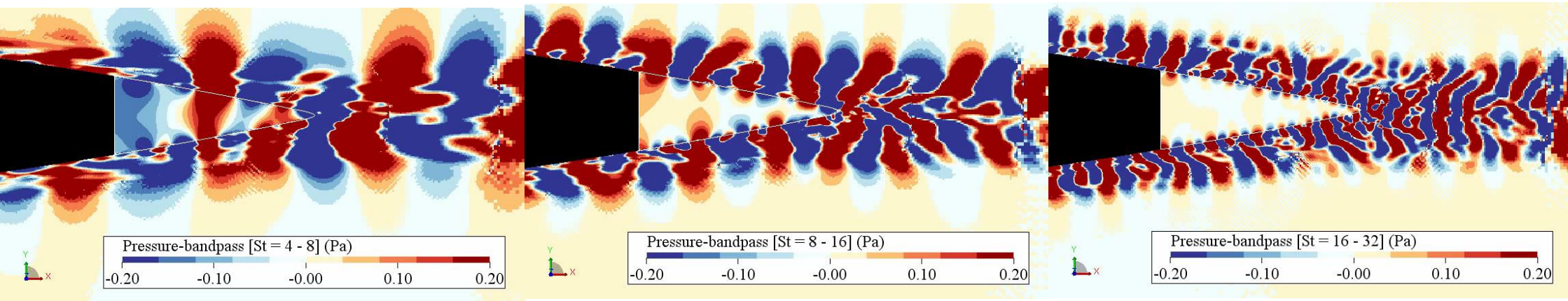


$$4 < St_c < 8$$

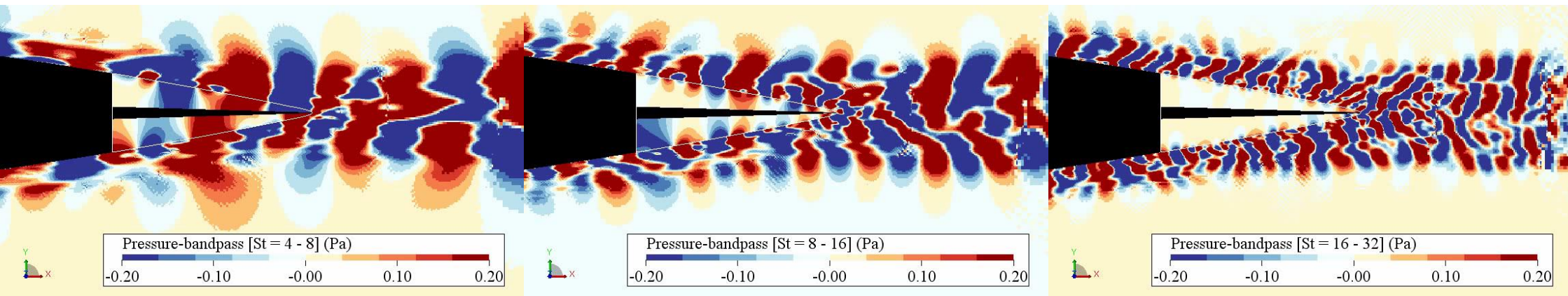
$$8 < St_c < 16$$

$$16 < St_c < 32$$

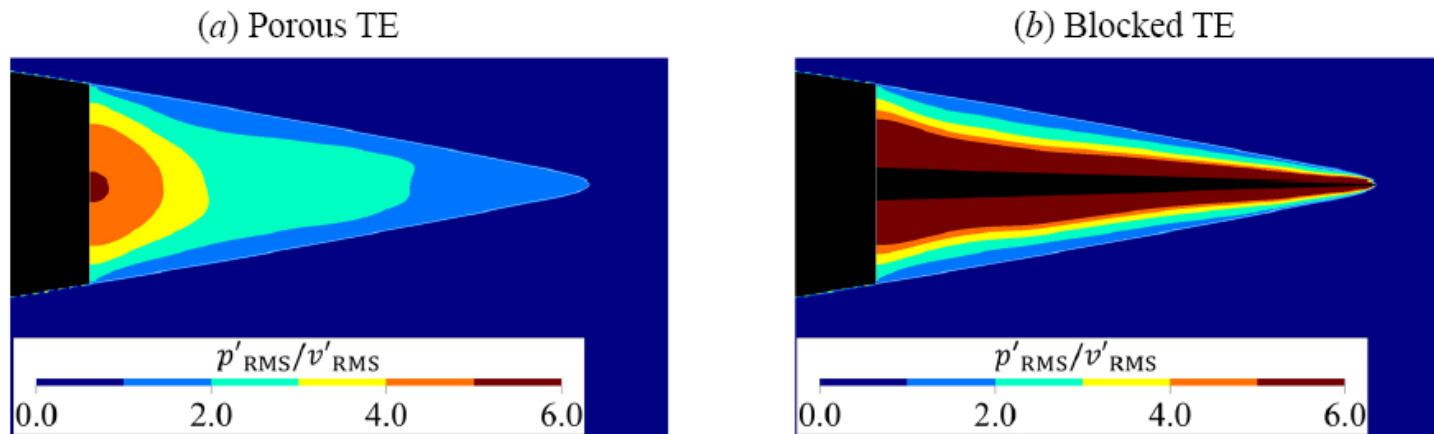
(a) Porous TE



(b) Blocked TE



- $p'_{RMS}/v'_{RMS}$  is proportional to the impedance of the porous material[1,2].



The comparison of  $p'_{RMS}/v'_{RMS}$  contour between porous and blocked TE

- Inside the porous TE, the ratio decreases in the streamwise direction, which appears to cause milder impedance jump at the actual trailing edge → **less efficient scattering at the trailing edge**.
- The variation of  $p'_{RMS}/v'_{RMS}$  in the porous TE might be interpreted as a continuous impedance mismatch → **acoustic scattering at multiple chordwise locations** [3].

[1] Maria, A. K., & James, C. J., "Acoustic absorption in porous materials", *Report No. NASA/TM, 316995*, 2011.

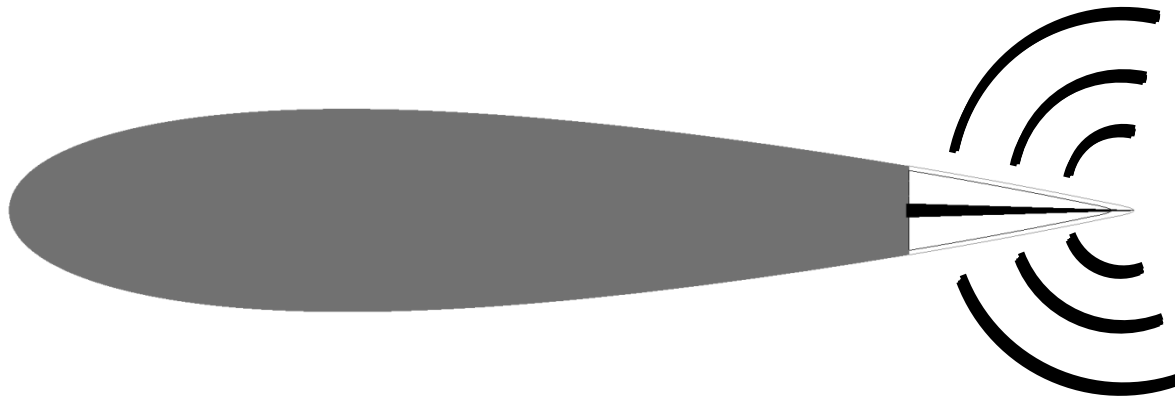
[2] Koh, S. R., Meinke, M., & Schröder, W., "Numerical analysis of the impact of permeability on trailing-edge noise". *Journal of Sound and Vibration*, 421, 348-376, 2018.

[3] Kisiil, A., & Ayton, L. J. Aerodynamic noise from rigid trailing edges with finite porous extensions. *Journal of Fluid Mechanics*, 836, 117-144, 2018.

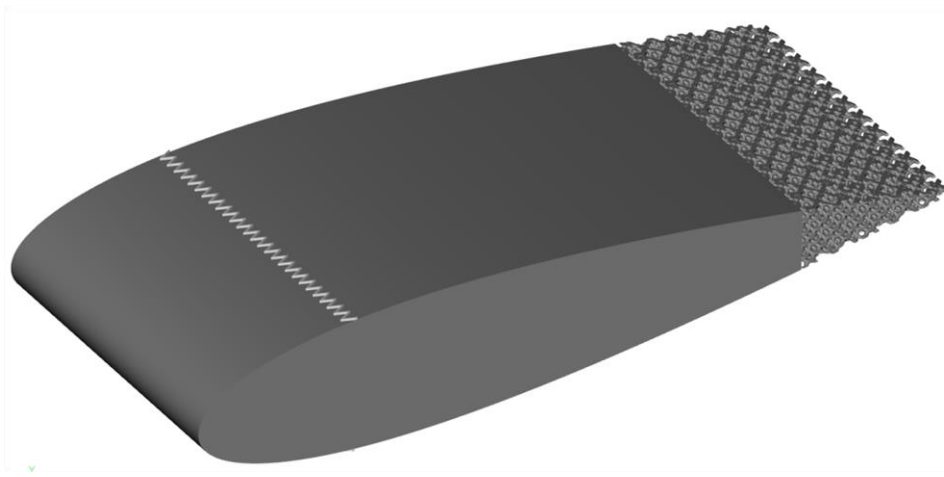


## VI. CONCLUSION & OUTLOOK

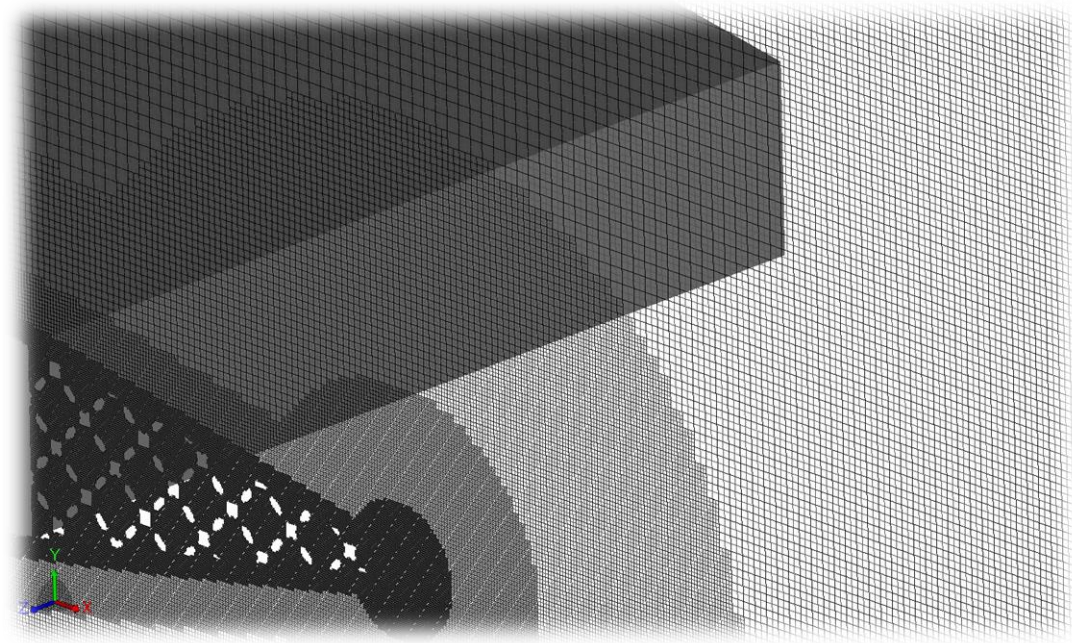
- The application of metal-foam to reduce trailing edge noise has been studied using lattice-Boltzmann method.
- Conventional solid trailing edge models can not be used directly to predict noise reduction of the porous TE.
- The flow-field interaction across the porous trailing edge is a necessary condition to achieve noise reduction.
- The noise reduction of the porous TE might be caused by the combination of **destructive interference between distributed sound sources** as well as the **reduction of scattering efficiency at the trailing edge**.



- Numerical study of a 3D-printed porous trailing edge for one-to-one comparison against the experiments.

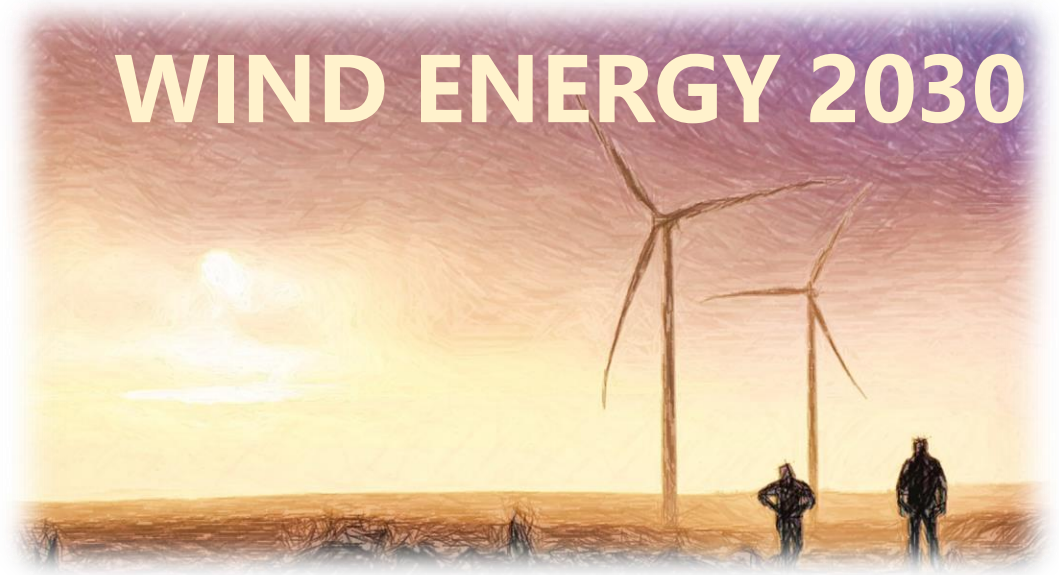


NACA 0018 with 3D-printed trailing edge



Mesh distribution in the simulation domain





# Thank you for your attention !

This study is supported by the project **SMARTANSWER** (Smart Mitigation of flow-induced **A**coustic Radiation and Transmission for reduced Aircraft, surface tra**N**Sport, **W**orkplaces and wind en**ER**gy noise) which has received funding from the European Unions Horizon 2020 research and innovation program under the **Marie Skodowska-Curie** grant agreement No. 722401. More information can be found on <https://www.h2020-smartanswer.eu/>